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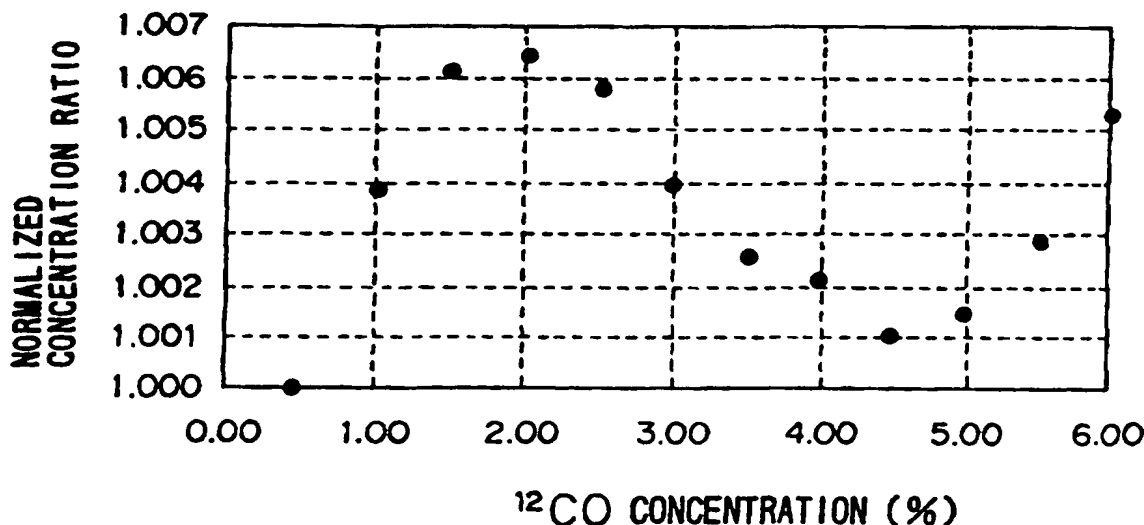
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## (57) Abstract

A correction curve is prepared by plotting <sup>12</sup>CO<sub>2</sub> concentrations and <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratios which are determined on the basis of a calibration curve and <sup>13</sup>CO<sub>2</sub> and <sup>12</sup>CO<sub>2</sub> absorbances of gaseous samples having the same <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio but known different <sup>12</sup>CO<sub>2</sub> concentrations. A gaseous test sample containing <sup>13</sup>CO<sub>2</sub> and <sup>12</sup>CO<sub>2</sub> as component gases is introduced into a cell, and spectrometrically measured. A <sup>12</sup>CO<sub>2</sub> concentration of the gaseous test sample is determined by way of the spectrometric measurement. A concentration ratio correction value is obtained on the basis of the correction curve and the <sup>12</sup>CO<sub>2</sub> concentration of the gaseous test sample thus determined. A measured <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio is divided by the concentration ratio correction value thus obtained for correction of the <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio. Thus, the measurement accuracy of the concentration ratios of the component gases can be improved.

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**DESCRIPTION****METHOD FOR SPECTROMETRICALLY MEASURING ISOTOPIC GAS AND  
APPARATUS THEREOF**5 **Technical Field**

The present invention relates to methods and apparatuses for spectrometrically measuring the concentration of an isotopic gas on the basis of a difference in the light absorption characteristics of the isotope.

10

**Background Art**

Isotopic analyses are useful for diagnosis of a disease in a medical application, in which metabolic functions of a living body can be determined by measuring a change in the concentration or concentration ratio of an isotope after administration of a drug containing the isotope. In the other fields, the isotopic analyses are used for studies of the photosynthesis and metabolism of plants, and for ecological tracing in a geochemical application.

20

It is generally known that gastric ulcer and gastritis are caused by bacteria called helicobacter pylori (HP) as well as by a stress. If the HP is present in the stomach of a patient, an antibiotic or the like should be administered to the patient for bacteria removal treatment. Therefore, it is indispensable to check if the patient has the HP. The HP has

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a strong urease activity for decomposing urea into carbon dioxide and ammonia.

Carbon has isotopes having mass numbers of 12, 13 and 14, among which  $^{13}\text{C}$  having a mass number of 13 is easy to handle because of its non-radioactivity and stability.

If the concentration of  $^{13}\text{CO}_2$  (a final metabolic product) or the concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  in breath of a patient is successfully measured after urea labeled with the isotope  $^{13}\text{C}$  is administered to the patient, the presence of the HP can be confirmed.

However, the concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  in naturally occurring carbon dioxide is 1:100. Therefore, it is difficult to determine the concentration ratio in the breath of the patient with high accuracy.

There have been known methods for determining the concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  by means of infrared spectroscopy (see JPB 61(1986)-42219 and JPB 61(1986)-42220).

In the method disclosed in JPB 61(1986)-42220, two cells respectively having a long path and a short path are provided, the path lengths of which are adjusted such that the light absorption by  $^{13}\text{CO}_2$  in one cell is equal to the light absorption by  $^{12}\text{CO}_2$  in the other cell. Light beams transmitted through the two cells are lead to spectrometric means, in which the light intensities are measured at wavelengths each providing the maximum sensitivity. In

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accordance with this method, the light absorption ratio can be adjusted to "1" for the concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  in naturally occurring carbon dioxide. If the concentration ratio is changed, the light absorption ratio also changes by the amount of a change in the concentration ratio. Thus, the change in the concentration ratio can be determined by measuring a change in the light absorption ratio.

(A) However, the method for determining the concentration ratio according to the aforesaid document suffers from the following drawbacks.

Calibration curves for determining the concentrations of  $^{12}\text{CO}_2$  should be prepared by using gaseous samples each having a known  $^{12}\text{CO}_2$  concentration.

To prepare the calibration curve for the  $^{12}\text{CO}_2$  concentration, the  $^{12}\text{CO}_2$  absorbances are measured for different  $^{12}\text{CO}_2$  concentrations. The  $^{12}\text{CO}_2$  concentrations and the  $^{12}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, and the calibration curve is determined by the method of least squares.

The calibration curve for the  $^{13}\text{CO}_2$  concentration is prepared in the same manner as described above.

For determination of the concentrations by means of infrared spectroscopy, the preparation of the calibration curves is based on an assumption that the relation between the concentration and the absorbance conforms to the Lambert-Beer

Law. However, the Lambert-Beer Law itself is an approximate expression. The actual relation between the concentration and the absorbance does not always conform to the Lambert-Beer Law. Therefore, all the plotted data do not perfectly fit to the calibration curve.

Fig. 1 is a graphical representation in which concentration ratios of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  are plotted with respect to  $^{12}\text{CO}_2$  concentrations, the  $^{12}\text{CO}_2$  concentrations and the  $^{13}\text{CO}_2$  concentrations having been determined by using calibration curves prepared on the basis of measurements of the absorbances of gaseous samples having the same concentration ratio ( $^{13}\text{CO}_2$  concentration/ $^{12}\text{CO}_2$  concentration = 1.077%) but different  $^{12}\text{CO}_2$  concentrations.

As shown in Fig. 1, the concentration ratios determined for different  $^{12}\text{CO}_2$  concentrations deviate from the actual concentration ratio (1.077%), and form an undulatory curve when plotted.

Although the cause of the deviation has not been elucidated yet, the deviation supposedly results from changes in the spectroscopic characteristics such as reflectance, refractive index and stray light in dependence on the  $^{12}\text{CO}_2$  concentration and from the error characteristics of the least square method employed for the preparation of the calibration curves.

If the concentration of a component gas is determined



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without correction of the characteristics associated with the deviation, a critical error may result.

(B) A variety of experiments have revealed that, where the infrared spectrometry is employed to measure the concentration of  $^{13}\text{CO}_2$  or the concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  (hereinafter referred to as " $^{13}\text{CO}_2$  concentration ratio"), measurement results differ from the actual  $^{13}\text{CO}_2$  concentration or  $^{13}\text{CO}_2$  concentration ratio depending on the concentration of oxygen contained in a gaseous sample.

Fig. 2 is a graphical representation in which  $^{13}\text{CO}_2$  concentration ratios are plotted with respect to oxygen contents, the  $^{13}\text{CO}_2$  concentration ratios having been determined by measuring gaseous samples containing  $^{13}\text{CO}_2$  diluted with oxygen and nitrogen and having the same  $^{13}\text{CO}_2$  concentration but different oxygen concentrations. The determined  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of a  $^{13}\text{CO}_2$  concentration ratio for an oxygen content of 0%.

As shown in Fig. 2, the  $^{13}\text{CO}_2$  concentration ratio is not constant but varies depending on the oxygen concentration.

If the  $^{13}\text{CO}_2$  concentration or the  $^{13}\text{CO}_2$  concentration ratio of a gaseous sample containing oxygen is measured in ignorance of this fact, it is obvious that a measurement differs from an actual value.

Fig. 3 is a graphical representation illustrating the

result of measurement in which gaseous samples having different  $^{13}\text{CO}_2$  concentration ratios and containing no oxygen were measured. In Fig. 3, the actual  $^{13}\text{CO}_2$  concentration ratios and the measured  $^{13}\text{CO}_2$  concentration ratios are plotted as abscissa and ordinate, respectively. The  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of the minimum  $^{13}\text{CO}_2$  concentration ratio.

Fig. 4 is a graphical representation illustrating the result of measurement in which gaseous samples having different  $^{13}\text{CO}_2$  concentration ratios and containing various concentration of oxygen (up to 90%) were measured. In Fig. 4, the actual  $^{13}\text{CO}_2$  concentration ratios and the measured  $^{13}\text{CO}_2$  concentration ratios are plotted as abscissa and ordinate, respectively. The  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of the minimum  $^{13}\text{CO}_2$  concentration ratio.

A comparison between the results shown in Figs. 3 and 4 indicates that the relationship between the actual  $^{13}\text{CO}_2$  concentration ratio and the measured  $^{13}\text{CO}_2$  concentration ratio in Fig. 3 is about 1:1 (or the slope of the fitting curve in Fig. 3 is about 1) while the relationship between the actual  $^{13}\text{CO}_2$  concentration ratio and the measured  $^{13}\text{CO}_2$  concentration ratio in Fig. 4 is about 1:0.3 (or the slope of the linear fitting curve in Fig. 4 is about 0.3).

Thus, the measurement of the  $^{13}\text{CO}_2$  concentration or the  $^{13}\text{CO}_2$  concentration ratio is influenced by the concentration

of oxygen contained in a gaseous sample, the cause of which has not been elucidated yet.

If the concentration or concentration ratio of a component gas is determined without performing a correction in consideration of the oxygen concentration, it is predicted that a critical error may result.

(C) Since the concentration of  $\text{CO}_2$ , particularly, the concentration of  $^{13}\text{CO}_2$  is extremely low, highly sensitive measurement is required. When the sensitivity of measurement is increased, a measured light intensity is responsive to changes in parameters of the measurement system, e.g., the light intensity of a light source, the temperature of a sample gas, the temperature of a cell to which the gas is introduced, the sensitivity of a photodetector and the like. Thus, the measured value may have an error caused by factors not related to the sample gas.

To solve this problem, the measurement is started after the measurement system is stabilized in a time-consuming manner. This reduces the operation efficiency and makes it impossible to meet a user demand to measure a large amount of samples in a short time.

For measurement of one breath sample, the  $^{12}\text{CO}_2$  absorbance is measured and the  $^{12}\text{CO}_2$  concentration is determined on the basis of a calibration curve for  $^{12}\text{CO}_2$ . The  $^{13}\text{CO}_2$  absorbance is measured and the  $^{13}\text{CO}_2$  concentration is

calculated on the basis of a calibration curve for  $^{13}\text{CO}_2$ , as well. The measurement of another breath sample is carried out in the same manner.

If the  $\text{CO}_2$  concentrations of the aforesaid two breath samples are at substantially the same level, the ranges of the calibration curves for  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  to be used for the concentration determination can be limited. Thus, the measurement accuracy can be increased by using limited ranges of the calibration curves.

(D) In a conventional infrared spectrometric method as described above, a bag containing a gaseous sample is connected to a predetermined pipe of a spectrometric apparatus, and the gaseous sample is introduced into a cell through the pipe by manually compressing the bag.

However, even small turbulence may drastically reduce the measurement accuracy because the absorbance of  $^{13}\text{CO}_2$  present in a trace amount is measured in the isotopic gas analysis. The gaseous sample cannot be passed through the cell at a constant flow rate by the manual compression of the bag. This generates a nonuniform flow of the gaseous sample in the cell and causes the gaseous sample to have a local temperature change and an incidental concentration change, thereby fluctuating a light detection signal.

The flow rate of the gaseous sample may be controlled to be constant by using a pump and a flow meter in combination.

However, the accuracy of the flow control cannot be ensured, because the volume of the bag containing the gaseous sample is small and the flow rate is low. Alternatively, an apparatus called mass flow meter for electronic flow control may be  
5 employed as flow control means. This improves the accuracy of the flow rate control, but results in a complicated apparatus and an increased cost.

(E) In the method disclosed in JPB 61(1986)-42220, the length of the cell is reduced and, therefore, a cell-absent space is  
10 filled with air. The air space hinders highly accurate measurement. If the lengths of paths between the light source and the cell and between the cell and the photoreceptor are increased, highly accurate measurement may be hindered.

More specifically, since the absorbance of  $^{13}\text{CO}_2$  present  
15 in a trace amount is measured in the isotopic gas measurement, even a small external disturbance reduces the measurement accuracy. A few percentage of  $^{12}\text{CO}_2$  and a trace amount of  $^{13}\text{CO}_2$  are present in the aforesaid air space and spaces between the light source and the cell and between the cell and  
20 the photoreceptor. A  $^{13}\text{CO}_2$  spectrum partially overlaps a  $^{12}\text{CO}_2$  spectrum and, if a filter is used, the band-pass width thereof influences the measurement. Therefore, the presence of  $^{12}\text{CO}_2$  indirectly influences the measurement of the  $^{13}\text{CO}_2$  absorbance, and the trace amount of  $^{13}\text{CO}_2$  directly influences  
25 the measurement of the  $^{13}\text{CO}_2$  absorbance.

To eliminate the influence of CO<sub>2</sub> present in a light path, an apparatus (see JPB 3(1991)-31218) has been proposed in which a light source, a sample cell, a reference cell, a interference filter, a detection element and like elements are  
5 accommodated in a sealed case which is connected to a column filled with a CO<sub>2</sub> absorbent through a tube and a circulation pump for circulating air within the sealed case and the column to remove CO<sub>2</sub> from the air in the sealed case.

The apparatus disclosed in this document can remove CO<sub>2</sub>  
10 which may adversely affect the measurement, but requires the column filled with the CO<sub>2</sub> absorbent, the tube and a large sealed case for accommodating the respective elements, resulting in a large-scale construction. In addition, the fabrication of the apparatus requires a laborious process such  
15 as for sealing the large case.

Further, a nonuniform flow of the air within the sealed case causes a local temperature change and an incidental concentration change, thereby causing a light detection signal to be fluctuated.

20 (F) In the infrared spectroscopic measurement, breath is sampled in breath sampling bags before and after a diagnostic drug is administered to a living body, and the breath samples in the breath sampling bags are respectively measured for determination of the <sup>13</sup>CO<sub>2</sub> concentration or the <sup>13</sup>CO<sub>2</sub>  
25 concentration ratio.

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The measurement of such breath samples is typically performed in a professional manner in a measurement organization, which manipulates a large amount of samples in a short time. Therefore, breath samples obtained before and  
5 after the drug administration are often mistakenly manipulated.

More specifically, breath samples obtained from one patient before and after the drug administration are mistaken for those obtained from another patient, or a breath sample  
10 obtained before the drug administration is mistaken for that obtained after the drug administration.

Such mistakes lead to erroneous measurement results and, therefore, should be assuredly prevented.

Further, if a breath sample includes a gas remaining in  
15 the oral cavity of a patient, the measurement accuracy is reduced. To reduce a measurement error, breath from the lung of the patient should be sampled.

Still further, since moisture in a breath sample adversely affects the optical measurement, the moisture should  
20 be removed from the breath sample. Furthermore, a consideration should be given to the breath sampling bag to prevent the breath sample from escaping from the bag.

#### Disclosure of Invention

25 It is an object of the present invention to provide a

method for spectrometrically measuring an isotopic gas, which is employed to precisely determine the concentration or concentration ratio of a component gas in a gaseous test sample containing a plurality of component gases by way of spectrometry when the gaseous test sample is introduced into a cell.

It is another object of the present invention to provide a method for spectrometrically measuring an isotopic gas, which is employed to precisely determine the concentration of a component gas in a gaseous test sample containing a plurality of component gases by way of spectrometry by using a limited range of a calibration curve when the gaseous test sample is introduced into a cell.

It is further another object of the present invention to provide a method for spectrometrically measuring an isotopic gas, which is employed to precisely determine the concentration or concentration ratio of  $^{13}\text{CO}_2$  contained in a gaseous test sample by way of spectrometry in consideration of the concentration of oxygen when the gaseous test sample into a cell.

It is still another object of the present invention to provide a method for spectrometrically measuring an isotopic gas, which is employed to precisely determine the concentration or concentration ratio of a component gas in a gaseous test sample containing a plurality of component gases



by way of spectrometry in such a manner that time-related influences on a measurement system can be minimized when the gaseous test sample is introduced into a cell.

It is yet another object of the present invention to  
5 provide an apparatus for spectrometrically measuring an isotopic gas, which has a simple construction and is capable of introducing a gaseous test sample containing a plurality of component gases at a constant flow rate for spectrometry.

It is still another object of the present invention to  
10 provide a breath sampling bag, which is given a consideration to assuredly prevent a breath sample from being mistakenly manipulated.

It is yet another object of the present invention to  
provide a breath sampling bag, which prevents the sampling of  
15 air present in the oral cavity of a patient but allows the sampling of breath from the lung of the patient.

It is still another object of the present invention to  
provide a breath sampling bag, which is capable of removing  
moisture from breath blown therein.

20 It is yet another object of the present invention to provide a breath sampling bag, which has a construction to prevent a breath sample from being escaped therefrom.

To achieve the aforesaid objects, the present invention provides a method for spectrometrically measuring an isotopic  
25 gas, which is described in claim 1.

In comparison with the prior-art method, the aforesaid method includes an additional step (the third step) of correcting the concentration ratio of a component gas in a gaseous test sample on the basis of the concentration of the component gas by using a correction curve prepared by measuring gaseous samples respectively containing the component gas in known concentrations or known concentration ratios. The correction of the concentration ratio eliminates the conventionally experienced drawback that the measured concentration ratios of the component gas which should basically be the same vary depending on the concentration of the component gas, thereby improving the measurement accuracy of the concentration ratio of the component gas.

Another method for spectrometrically measuring an isotopic gas in accordance with the present invention is described in claim 4.

In this method, the concentration of a component gas is tentatively determined with the use of a calibration curve which is prepared on the basis of data obtained by measuring gaseous samples containing the component gas in known concentrations within a predetermined range (the second step). However, all the data do not perfectly fit to the calibration curve on which the tentatively determined concentration of the component gas is based, as described in "Background Art".

For this reason, another calibration curve is prepared by

using some of the data within a limited range around the concentration of the component gas determined in the second step. It is confirmed that part of the calibration curve prepared on the basis of the data in the narrower range  
5 strictly conforms to the Lambert-Beer Law. Therefore, the concentration of the component gas is determined on the basis of the absorbance thereof by using the calibration curve thus prepared (the third step).

Since the accuracy of the calibration curve is improved  
10 over the prior art method, the obtained concentration of the component gas is more accurate. Thus, the measurement accuracy of the concentration of the component gas can be increased.

Further another method for spectrometrically measuring an  
15 isotopic gas in accordance with the present invention is described in claim 6 or 7.

In comparison with the prior art method, the aforesaid method includes an additional step (the third step) of correcting the concentration or concentration ratio of a  
20 component gas in a gaseous test sample on the basis of a measured oxygen concentration of the gaseous test sample by using a correction curve prepared by measuring gaseous samples respectively containing oxygen in known concentrations.

The correction eliminates the newly encountered drawback  
25 that the measured concentrations of the component gas which

should basically be the same vary depending on the oxygen concentration, thereby improving the measurement accuracy of the concentration or concentration ratio of the component gas.

5 The oxygen concentration may be determined by means of any of various oxygen sensors or by spectrometrically measuring an absorbance in an oxygen molecular spectrum.

Still another method for spectrometrically measuring an isotopic gas in accordance with the present invention is described in claim 8.

10 It is a conventional practice that a reference gas measurement in which a light intensity is measured with a reference gas filled in a cell and a sample measurement in which a light intensity is measured with a gaseous sample filled in the cell are each performed once for measurement of an  
15 absorbance. In the aforesaid method, however, the absorbance is determined on the basis of the light intensity measured in the sample measurement and an average of light intensity measured in the reference gas measurements performed before and after the sample measurement.

20 Therefore, a time-related variation of the absorbances measured before and after the sample measurement can be corrected by using the average of the light intensity obtained in the reference gas measurement. Thus, an influence of the time-related change of the measurement system can be  
25 eliminated.

The result of the reference gas measurement performed after the sample measurement can serve as the result of the reference gas measurement performed before the next sample measurement. Therefore, one measurement result for the  
5 reference gas can be used twice.

Yet another method for spectrometrically measuring an isotopic gas in accordance with the present invention is described in claim 10.

In this method, an absorbance is determined on the basis  
10 of a light intensity measured in a reference gas measurement and an average of light intensity measured in sample measurements performed before and after the reference gas measurement.

Since the measurement should be performed twice on the same gaseous sample, the operation efficiency is reduced.  
15 However, a time-related variation of the absorbances obtained before and after the sample measurement can be corrected by using the average of the light intensity obtained in the sample measurement. Thus, an influence of the time-related change of the measurement system can be eliminated.

20 Still another method for spectrometrically measuring an isotopic gas in accordance with the present invention is described in claim 12.

In this method, two breath test samples can be measured on condition that the CO<sub>2</sub> concentrations thereof are at the  
25 same level and, therefore, a range of a calibration curve to

be used can be limited. The accuracy of the measurement can be improved as the range of the calibration curve to be used becomes narrower. Hence, the measurement accuracy can be improved by using a limited range of the calibration curve.

5 Yet another method for spectrometrically measuring an isotopic gas in accordance with the present invention is described in claim 13 or 14. This method is based on a premise that a first gaseous sample is filled in a cell for light intensity measurement thereof and, after the first gaseous  
10 sample is discharged from the cell, a second gaseous sample is filled in the same cell for light intensity measurement thereof.

To achieve the aforesaid objects, the present invention provides an apparatus for spectrometrically measuring an isotopic gas, which includes a gas injection means for sucking  
15 therein a gaseous sample and then injecting the gaseous sample into a cell by mechanically pushing out the gaseous sample at a constant flow rate (claim 15).

With this construction, the gaseous sample is injected into the cell at a constant flow rate. Therefore, the gaseous  
20 sample uniformly flows within the cell, so that a highly accurate light detection signal free from fluctuation can be provided for more accurate concentration measurement.

Usable as the gas injection means for mechanically pushing out the gaseous sample at the constant rate is, for  
25 example, a mechanism including a piston and a cylinder and

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adapted to move the cylinder at a constant rate.

In accordance with another aspect of the present invention, the apparatus for spectrometrically measuring an isotopic gas further includes a temperature maintaining means  
5 for maintaining a cell for receiving the gaseous sample introduced therein at a constant temperature (claim 16).

By keeping the temperature within the cell constant, the temperature condition of the gaseous sample can be kept uniform, so that a highly accurate light detection signal free  
10 from fluctuation can be provided.

To achieve the aforesaid objects, the present invention provides another apparatus for spectrometrically measuring an isotopic gas, which includes a cell for receiving a gaseous sample introduced therein positioned in the midst of a light  
15 path between a light source and a photoreceptor, and a reference cell disposed in a portion of the light path not occupied by the cell and filled with a reference gas having no absorption at a wavelength for measurement (claim 17).

Where a measuring vessel is not provided with the  
20 reference cell and filled with air which contains component gases of the same kinds as contained in the gaseous sample, an adverse effect is caused due to the component gases present in the measuring vessel. With the aforesaid construction, however, the reference cell filled with the reference gas  
25 having no absorption at the measurement wavelength is disposed

in the light path, thereby eliminating the optically adverse effect. Thus, the concentration measurement can be performed more accurately.

Further another apparatus for spectrometrically measuring  
5 an isotopic gas in accordance with the present invention  
includes two cells each disposed parallel to a light path  
between a light source and a photoreceptor and having  
different lengths for receiving a gaseous sample introduced  
therein, and a reference cell disposed between a shorter one  
10 of the two cells and the photoreceptor or between the shorter  
cell and the light source and filled with a reference gas  
having no absorption at a wavelength for measurement (claim  
20).

With the cells having different lengths, a large space is  
15 present between the shorter cell and the photoreceptor or  
between the light source and the shorter cell, and component  
gases of the same kinds as contained in the gaseous sample are  
present in the space and adversely affect the optical  
measurement. More accurate concentration measurement can be  
20 ensured by providing in the space the reference cell filled  
with the reference gas having no absorption at the measurement  
wavelength.

In accordance with further another aspect of the present  
invention, the aforesaid apparatuses for spectrometrically  
25 measuring an isotopic gas each further include a gas flow



generating means for constantly passing the reference gas through the reference cell at a constant flow rate (claims 18 and 21).

5 The passing of the reference gas through the reference cell is based on the following consideration. If the reference cell is sealed with the reference gas filled therein, the reference gas gradually leaks from a joint of the cell and is replaced with outside air. The air which has entered the cell contains component gases of the same kinds as  
10 contained in the gaseous sample, resulting in an optically adverse effect. Further, the reference gas constantly flowing at a constant rate does not generate a nonuniform gas flow within the reference cell, thereby preventing a light detection signal from being fluctuated.

15 The gas flow generating means may comprise a valve for introducing the reference gas from a gas container, a pipe and a flow meter, for example.

In accordance with yet another aspect of the present invention, the aforesaid apparatus for spectrometrically  
20 measuring an isotopic gas further includes a temperature maintaining means for maintaining the cell for receiving the gaseous sample introduced therein and the reference cell at a constant temperature (claims 19 and 22).

By keeping the temperature within the cell and the  
25 reference cell constant, a temperature difference between the

gaseous sample and the reference gas can be eliminated, so that the thermal conditions of the gaseous sample and the reference gas can be kept equivalent. Thus, the absorbances can be determined accurately.

5       To achieve the aforesaid objects, the present invention provides a breath sampling bag, which includes a plurality of breath accumulating chambers joined together for respectively accumulating a plurality of breath samples, and a plurality of breath introduction pipes for respectively introducing the  
10   breath samples from the plurality of breath accumulating chambers into a plurality of inlets of a gas measuring apparatus for measuring a breath sample, the plurality of breath introduction pipes each being configured such as to be prevented from being connected to the inlets of the gas  
15   measuring apparatus in a wrong way (claim 23).

      A gas measuring apparatus in accordance with the present invention is adapted to measure breath samples contained in a breath sampling bag which includes a plurality of breath accumulating chambers joined together and a plurality of  
20   breath introduction pipes for introducing therethrough a plurality of breath samples from a living body into the respective breath accumulating chambers, and includes a plurality of breath inlets for respectively introducing the breath samples from the breath accumulating chambers through  
25   the breath introduction pipes, the plurality of breath inlets

each being configured such as to prevent the breath introduction pipes from being connected thereto in a wrong way (claim 24).

5 With the breath sampling bag and gas measuring apparatus of the aforesaid constructions, such an inconvenient accident can be eliminated that one breath sample in one breath accumulating chamber of the breath sampling bag is introduced into the gas measuring apparatus mistakenly for another breath sample in another breath accumulating chamber.

10 Where breath is sampled from a living body before and after a diagnostic drug is administered to the living body and the  $^{13}\text{CO}_2$  concentration or  $^{13}\text{CO}_2$  concentration ratio of the breath samples is measured, for example, the manipulation mistake of the breath samples obtained before and after the  
15 administration of the diagnostic drug for measurement can be prevented. Further, where a load test is performed and breath is sampled at a predetermined time interval after the  
administration of a diagnostic drug, breath samples thus  
obtained are prevented from being measured in a wrong order.

20 The breath introduction pipes or the breath inlets are, for example, asymmetrically configured for prevention of the connection mistake of the breath sampling bag. For asymmetrical configuration, the plurality of breath introduction pipes may have different diameters, lengths and  
25 cross-sections, and the plurality of breath inlets may have

different diameters, lengths and cross-sections corresponding to those of the respective breath introduction pipes.

Another breath sampling bag in accordance with the present invention includes a breath accumulating chamber for accumulating breath and a breath introduction pipe for  
5 introducing the breath from a living body into the breath accumulating chamber, the breath introduction pipe having a resistance generating means for generating a resistance to the blowing of the breath during the sampling of the breath (claim  
10 25).

With this construction, the provision of the resistance generating means prevents the sampling of breath present in the oral cavity of the living body, but enables the sampling of breath from the lung thereof. Thus, a measurement error  
15 can be reduced.

The resistance generating means is embodied by allowing the interior of the breath introduction pipe to have some change which generates a resistance to the blowing of the breath. For example, the inner diameter of the breath  
20 introduction pipe may be reduced or, alternatively, a resistance component may be provided on the interior of the breath introduction pipe.

Further another breath sampling bag in accordance with the present invention includes a breath accumulating chamber  
25 for accumulating breath and a breath introduction pipe for

introducing the breath from a living body into the breath accumulating chamber, the breath introduction pipe having a detachable filter for removing moisture from the breath during the sampling of the breath (claim 26).

5        With this construction, the moisture in the breath can be removed therefrom by means of the filter, so that a reduction in the optical measurement accuracy can be prevented. The removal of moisture is particularly effective for infrared spectrometry.

10       Still another breath sampling bag in accordance with the present invention includes a breath accumulating chamber for accumulating breath and a breath introduction pipe for introducing the breath from a living body into the breath accumulating chamber, the breath introduction pipe having a  
15       valve for preventing the back flow of the breath during the sampling of the breath (claim 27).

      With this construction, the provision of the back-flow prevention valve in the breath introduction pipe prevents the breath from leaking out of the breath sampling bag.

20       Another gas measuring apparatus in accordance with the present invention, which is adapted to measure a breath sample contained in a breath sampling bag including a breath accumulating chamber for accumulating the breath sample and a breath introduction pipe with a back-flow prevention valve for  
25       introducing the breath sample from a living body into the

breath accumulating chamber, includes a breath inlet for introducing therein the breath sample from the breath sampling bag through the breath introduction pipe, the breath inlet having means for disabling the function of the valve with the  
5 breath introduction pipe being connected to the breath inlet (claim 28).

With this construction, the function of the valve can be disabled with the breath introduction pipe being connected to the breath inlet when the breath sample is to be introduced  
10 into the gas measuring apparatus through the breath introduction pipe. Therefore, the breath sample can be smoothly introduced into the gas measuring apparatus.

The means for disabling the function of the valve is embodied, for example, by providing a long pin projecting from  
15 the breath inlet, which is adapted to forcibly open the valve when the breath introduction pipe is connected to the breath inlet.

The foregoing and other objects and features of the present invention will become apparent from the following  
20 description with reference to the attached drawings.

#### Brief Description of Drawings

Hereinafter, concentration of  $^{12}\text{CO}_2$  is called " $^{12}\text{Conc}$ ", concentration of  $^{13}\text{CO}_2$  is called " $^{13}\text{Conc}$ ", absorbance of  $^{12}\text{CO}_2$   
25 is called " $^{12}\text{Abs}$ " and absorbance of  $^{13}\text{CO}_2$  is called " $^{13}\text{Abs}$ ".

Fig. 1 is a graphical representation in which concentrations  $^{12}\text{Conc}$  and concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  are plotted as abscissa and ordinate, respectively, the concentrations  $^{12}\text{Conc}$  and  $^{13}\text{Conc}$  and the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  having been determined by using calibration curves prepared on the basis of measurements of the absorbances  $^{12}\text{Abs}$  and  $^{13}\text{Abs}$  of component gases in gaseous samples having the same concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$  but different concentrations of the component gases;

Fig. 2 is a graphical representation in which  $^{13}\text{CO}_2$  concentration ratios are plotted with respect to oxygen contents, the  $^{13}\text{CO}_2$  concentration ratios having been determined by measuring gaseous samples containing  $^{13}\text{CO}_2$  diluted with oxygen and nitrogen and having the same  $^{13}\text{CO}_2$  concentration ratio but different oxygen concentrations, the  $^{13}\text{CO}_2$  concentration ratios being normalized on the basis of a  $^{13}\text{CO}_2$  concentration ratio for an oxygen content of 0%;

Fig. 3 is a graphical representation illustrating the result of measurement in which gaseous samples having different  $^{13}\text{CO}_2$  concentration ratios and containing no oxygen were measured, in which graphical representation the actual  $^{13}\text{CO}_2$  concentration ratios and the measured  $^{13}\text{CO}_2$  concentration ratios are plotted as abscissa and ordinate, respectively, and the  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of the minimum  $^{13}\text{CO}_2$  concentration

ratio;

Fig. 4 is a graphical representation illustrating the result of measurement in which gaseous samples having different  $^{13}\text{CO}_2$  concentration ratios and containing various concentration of oxygen (up to 90%) were measured, in which graphical representation the actual  $^{13}\text{CO}_2$  concentration ratios and the measured  $^{13}\text{CO}_2$  concentration ratios are plotted as abscissa and ordinate, respectively, and the  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of the minimum  $^{13}\text{CO}_2$  concentration ratio;

Fig. 5 is a view illustrating the appearance of a breath sampling bag to be connected to nozzles of an apparatus for spectrometrically measuring an isotopic gas;

Fig. 6 is a partial view illustrating pipes connected to an end of the breath sampling bag;

Fig. 7 is a block diagram illustrating the overall construction of the spectrometric apparatus;

Fig. 8 is a sectional view illustrating the construction of a cell chamber 11;

Fig. 9 is a block diagram schematically illustrating a mechanism for adjusting the temperature of the cell chamber;

Figs. 10A and 10B are a plan view and a side view, respectively, of a gas injector for quantitatively injecting a gaseous sample;

Fig. 11 is a diagram illustrating a gas flow path through



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which a clean reference gas is passed for cleaning the gas flow path and the cell chamber of the spectrometric apparatus;

Fig. 12 is a diagram illustrating a gas flow path through which the clean reference gas is passed for cleaning the gas flow path and the cell chamber of the spectrometric apparatus  
5 and for performing a reference measurement;

Fig. 13 is a diagram illustrating a state where a base gas is sucked from a breath sampling bag by means of the gas injector 21 with the reference gas prevented from flowing  
10 through first and second sample cells 11a and 11b;

Fig. 14 is a diagram illustrating a gas flow path to be employed when the base gas sucked in the gas injector 21 is mechanically pushed out at a constant rate by the gas injector 21 for measurement of light intensity by detection elements 25a  
15 and 25b;

Fig. 15 is a diagram illustrating a state where a sample gas is sucked from the breath sampling bag by means of the gas injector 21 with the reference gas prevented from flowing through the first and second sample cells 11a and 11b;

Fig. 16 is a diagram illustrating a gas flow path to be employed when the sample gas sucked in the gas injector 21 is mechanically pushed out at a constant rate by the gas injector 21 for measurement of light intensity by the detection elements 25a and 25b;  
20

Fig. 17A is a graphical representation in which  $^{12}\text{CO}_2$   
25

concentrations and  $^{12}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, for preparation of a calibration curve, the  $^{12}\text{CO}_2$  absorbances having been measured for 20 measuring points in a  $^{12}\text{CO}_2$  concentration range of about 0% to about 6%;

Fig. 17B is a graphical representation in which  $^{12}\text{CO}_2$  concentrations and  $^{12}\text{CO}_2$  absorbances in five data points in a relatively narrow  $^{12}\text{CO}_2$  concentration range around a  $^{12}\text{CO}_2$  concentration determined by using the calibration curve of Fig. 17A are plotted as abscissa and ordinate, respectively;

Fig. 18A is a graphical representation in which  $^{13}\text{CO}_2$  concentrations and  $^{13}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, for preparation of a calibration curve, the  $^{13}\text{CO}_2$  absorbances having been measured for 20 measuring points in a  $^{13}\text{CO}_2$  concentration range of about 0.00% to about 0.07%;

Fig. 18B is a graphical representation in which  $^{13}\text{CO}_2$  concentrations and  $^{13}\text{CO}_2$  absorbances in five data points in a relatively narrow  $^{13}\text{CO}_2$  concentration range around a  $^{13}\text{CO}_2$  concentration determined by using the calibration curve of Fig. 18A are plotted as abscissa and ordinate, respectively;

Fig. 19 is a graphical representation in which concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  plotted as ordinate are normalized on the basis of a concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$  obtained when  $^{12}\text{Conc}$  is 0.5%;

Fig. 20 is a graphical representation illustrating the relationship of  $^{12}\text{C}$ Conc (plotted as abscissa) versus  $^{13}\text{CO}_2$  concentration ratio  $^{13}\text{C}/^{12}\text{C}$  (plotted as ordinate) which was determined by measuring the  $^{12}\text{CO}_2$  concentrations  $^{12}\text{C}$ Conc and  $^{13}\text{CO}_2$  concentrations  $^{13}\text{C}$ Conc of gaseous samples;

Fig. 21 is a graphical representation illustrating the relationship of  $^{12}\text{C}$ Conc (plotted as abscissa) versus concentration ratio  $^{13}\text{C}/^{12}\text{C}$  (plotted as ordinate) which was determined by measuring the  $^{12}\text{CO}_2$  concentrations  $^{12}\text{C}$ Conc and  $^{13}\text{CO}_2$  concentrations  $^{13}\text{C}$ Conc of gaseous samples and correcting obtained concentration ratios  $^{13}\text{C}/^{12}\text{C}$ ;

Fig. 22 is a graphical representation illustrating the relationship of  $^{12}\text{C}$ Conc (plotted as abscissa) versus concentration ratio  $^{13}\text{C}/^{12}\text{C}$  (plotted as ordinate) which was obtained by determining the  $^{12}\text{CO}_2$  concentrations  $^{12}\text{C}$ Conc and  $^{13}\text{CO}_2$  concentrations  $^{13}\text{C}$ Conc of gaseous samples on the basis of absorbances measured on the gaseous samples by using the calibration curves shown in Figs. 17A and 18A;

Fig. 23 is a graphical representation illustrating the relationship of  $^{12}\text{C}$ Conc (plotted as abscissa) and concentration ratio  $^{13}\text{C}/^{12}\text{C}$  (plotted as ordinate) which was obtained by determining the concentration

ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  of gaseous samples first on the basis of the calibration curves shown in Figs. 17A and 18A and then on the basis of the calibration curves in limited ranges shown in Figs. 17B and 18B; and

5        Fig. 24 is a graphical representation illustrating the result of measurement in which gaseous samples having different  $^{13}\text{CO}_2$  concentration ratios and containing various concentration of oxygen (up to 90%) were measured and measurements were subjected to a correction process according  
10      to the present invention, in which graphical representation the actual  $^{13}\text{CO}_2$  concentration ratios and the measured  $^{13}\text{CO}_2$  concentration ratios are plotted as abscissa and ordinate, respectively, and the  $^{13}\text{CO}_2$  concentration ratios are normalized on the basis of the minimum  $^{13}\text{CO}_2$  concentration  
15      ratio.

#### Best Mode for Carrying Out the Invention

A preferred embodiment of the present invention will hereinafter be described with reference to the attached  
20      drawings. The embodiment is adapted for a case where a  $^{13}\text{CO}_2$  concentration or concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$  in a breath test sample is spectrometrically determined after administration of an urea diagnostic drug labeled with an isotope  $^{13}\text{C}$ .

#### 25      I. Breath test

Before the urea diagnostic drug is administered to a patient, breath of the patient is sampled in a breath sampling bag. The volume of the breath sampling bag may be about 250ml. Then, the urea diagnostic drug is administered to the patient and, after a lapse of 10 to 15 minutes, breath of the patient is sampled in the breath sampling bag in the same manner as in the previous breath sampling.

Fig. 5 is a view illustrating the appearance of the breath sampling bag 1 to be connected to nozzles  $N_1$  and  $N_2$  of an apparatus for spectrometrically measuring an isotopic gas. The breath sampling bag 1 includes a breath sampling chamber 1a for sampling breath of the patient after the administration of the urea diagnostic drug and a breath sampling chamber 1b for sampling breath of the patient before the administration of the urea diagnostic drug, the breath sampling chambers 1a and 1b being integrally molded and joined together to form a single body.

A pipe 2a is attached to an end of the breath sampling chamber 1a, and a pipe 2b is attached to an end of the breath sampling chamber 1b. Bottom ends 5a and 5b of the breath sampling chambers 1a and 1b are closed. The pipes 2a and 2b each have two functions, i.e., the pipes 2a and 2b serve not only as breath blowing ports from which breath is blown into the breath sampling chambers 1a and 1b, but also for introducing the breath samples from the breath sampling

chambers 1a and 1b into the spectrometric apparatus when the breath sampling bag is connected to the nozzles  $N_1$  and  $N_2$  of the apparatus.

When breath is sampled, a cylindrical filter (like  
5 cigarette filter) 7a or 7b is fitted into the pipe 2a or 2b, and then the breath is blown into the breath sampling bag 1. The filters 7a and 7b are used to remove moisture in the breath.

As shown in Fig. 6, back-flow valves 3a and 3b are  
10 provided in the pipes 2a and 2b, respectively, for preventing the breath blown into the breath sampling bag from flowing back.

The pipes 2a and 2b each have a portion having a smaller inner diameter (e.g., a smaller diameter portion 4a or 4b) for  
15 generating a resistance to the blowing of the breath. The resistance to the blowing of the breath allows the patient to exhale air from his lung. It has been experimentally confirmed that air exhaled from the lung of a patient provides a more stable  $CO_2$  concentration than air present in the oral  
20 cavity of the patient.

After the completion of the sampling of the breath, the filters are removed, and the pipes 2a and 2b are inserted into the nozzles  $N_1$  and  $N_2$ , respectively, of the spectrometric  
25 apparatus. The nozzles  $N_1$  and  $N_2$  have different inner diameters, and the pipes 2a and 2b have different outer

diameters corresponding to the inner diameters of the nozzles  $N_1$  and  $N_2$ . This prevents the pipes 2a and 2b from being inserted into wrong nozzles  $N_2$  and  $N_1$ , thereby preventing the breath samples obtained before and after the administration of the urea diagnostic drug from being mistakenly manipulated.

The nozzles  $N_1$  and  $N_2$  of the spectrometric apparatus have projections 6a and 6b, respectively, which are adapted to disable the function of the back-flow valves 3a and 3b when the pipes 2a and 2b are inserted into the nozzles  $N_1$  and  $N_2$ .

Although the outer diameters of the pipes 2a and 2b are made different in this embodiment, any other constructions may be employed to prevent the mistake of connection between the pipes 2a and 2b and the nozzles  $N_1$  and  $N_2$ . For example, the pipes may have different lengths and the nozzles  $N_1$  and  $N_2$  of the spectrometric apparatus may have different depths corresponding to the lengths of the pipes. With this construction, a longer one of the pipes mistakenly inserted into a nozzle having a smaller depth fails to perfectly fit in the nozzle. Therefore, a user notices the connection mistake of the pipes. Alternatively, the pipes may have different cross sections (e.g., round, rectangular or triangular cross sections).

Upon completion of the connection of the breath sampling bag 1, the spectrometric apparatus performs the following automatic control.

## II. Apparatus for spectrometrically measuring isotopic gas

Fig. 7 is a block diagram illustrating the overall construction of the apparatus for spectrometrically measuring an isotopic gas.

5        The breath sampling bag is set to the apparatus so that one breath sampling chamber thereof containing the breath sampled after the drug administration (hereinafter referred to as "sample gas") and the other breath sampling chamber thereof containing the breath (hereinafter referred to as "base gas")  
10        sampled before the drug administration are connected to the nozzles  $N_1$  and  $N_2$ , respectively. The nozzle  $N_1$  is connected to one port of a three-way valve  $V_1$  through a transparent resin pipe (hereinafter referred to simply as "pipe") and the nozzle  $N_2$  is connected to one port of a three-way valve  $V_2$   
15        through a pipe.

A reference gas (any gas having no absorption at a wavelength for measurement, e.g., nitrogen gas) is supplied from a gas cylinder to the apparatus. The reference gas flows through a flow path diverged into two paths. One path is  
20        connected through a flow meter  $M_1$  to a reference cell 11c. The other path is connected through a flow meter  $M_2$  to one port of a three-way valve  $V_3$ . The reference gas flows into the reference cell 11c, and discharged therefrom.

The other ports of the three-way valve  $V_3$  are connected  
25        to another port of the three-way valve  $V_1$  and to a first



sample cell 11a for measuring a  $^{12}\text{CO}_2$  absorbance. The other ports of the three-way valve  $V_2$  are connected to the first sample cell 11a through a two-way valve  $V_4$  and to the other port of the three-way valve  $V_1$ .

5        A gas injector 21 (volume: 60cc) for quantitatively injecting the sample gas or the base gas is interposed between the three-way valve  $V_3$  and the first sample cell 11a. The gas injector 21 is a syringe-like device having a piston and a cylinder. The piston is driven by cooperation of a motor, a  
10       screw connected to the motor and a nut fixed to the piston (which will be described later).

As shown in Fig. 7, a cell chamber 11 has the first sample cell 11a having a smaller length for measuring therein a  $^{12}\text{CO}_2$  absorbance, a second sample cell 11b having a greater  
15       length for measuring therein a  $^{13}\text{CO}_2$  absorbance, and the reference cell 11c through which the reference gas is passed. The first sample cell 11a communicates with the second sample cell 11b. The sample gas or the base gas is introduced into the first sample cell 11a and then into the second cell 11b,  
20       and discharged therefrom. The reference gas is introduced into the reference cell 11c, and then discharged therefrom. Specifically, the first and second sample cells 11a and 11b have lengths of 13mm and 250mm, respectively, and the reference cell 11c has a length of 236mm.

25       A discharge pipe extending from the second sample cell

11b is provided with an O<sub>2</sub> sensor 18. Usable as the O<sub>2</sub> sensor 18 are commercially available oxygen sensors such as a solid electrolyte gas sensor (e.g., zirconia sensor) and an electrochemical gas sensor (e.g., galvanic cell sensor).

5        A reference character L denotes an infrared light source having two waveguides 23a and 23b for guiding infrared rays for irradiation. The generation of the infrared rays may be achieved in any way. For example, a ceramic heater (surface temperature: 450°C) and the like can be used. A rotary  
10    chopper 22 for periodically blocking the infrared rays is provided adjacent to the infrared light source L. Infrared rays emitted from the infrared light source L are transmitted to the first sample cell 11a and the reference cell 11c through a first light path, and to the second sample cell 11b  
15    through a second light path (see Fig. 8).

      A reference character D denotes an infrared detector for detecting the infrared rays transmitted through the cells. The infrared detector D has a first wavelength filter 24a and a first detection element 25a disposed in the first light  
20    path, and a second wavelength filter 24b and a second detection element 25b disposed in the second light path.

      The first wavelength filter 24a (band width: about 20nm) passes an infrared ray having a wavelength of about 4,280nm to be used for measurement of a <sup>12</sup>CO<sub>2</sub> absorbance. The second  
25    wavelength filter 24b (band width: about 50nm) passes an

infrared ray having a wavelength of about 4,412nm to be used for measurement of a  $^{13}\text{CO}_2$  absorbance. Usable as the first and second detection elements 25a and 25b are any elements capable of detecting infrared rays. For example, a  
5 semiconductor infrared sensor such as of PbSe is used.

The first wavelength filter 24a and the first detection element 25a are housed in a package 26a filled with an inert gas such as Ar. Similarly, the second wavelength filter 24b and the second detection element 25b are housed in a package  
10 26b filled with an inert gas.

The whole infrared detector D is maintained at a constant temperature (25°C) by means of a heater and a Peltier element. The inside temperatures of the packages 26a and 26b are kept at 0°C by means of a Peltier element.

15 The cell chamber 11 is formed of a stainless steel, and vertically and laterally sandwiched between metal plates (e.g., brass plates) 12. A heater 13 is provided on upper, lower and lateral sides of the cell chamber. The cell chamber 11 is sealed with insulators 14 such as of polystyrene foam  
20 with the heater 13 interposed therebetween. Though not shown, a temperature sensor (e.g., a platinum temperature sensor) for measuring the temperature of the cell chamber 11 is provided in the cell chamber 11.

The cell chamber 11 has two tiers. The first sample cell  
25 11a and the reference cell 11c are disposed in one tier, and

the second sample cell 11b is disposed in the other tier.

The first light path extends through the first sample cell 11a and the reference cell 11c which are disposed in series, and the second light path extends through the second sample cell b. Reference characters 15, 16 and 17 denote sapphire transmission windows through which the infrared rays are transmitted.

Fig. 9 is a block diagram illustrating a mechanism for adjusting the temperature of the cell chamber 11. The temperature adjustment mechanism is constituted by the temperature sensor 32 provided in the cell chamber 11, a temperature adjustment substrate 31 and the heater 13. The temperature of the temperature adjustment substrate 31 may be adjusted in any manner. For example, the temperature adjustment can be achieved by changing the duty ratio of a pulse current flowing through the heater 13 on the basis of a temperature measurement signal of the temperature sensor 32. The heater 13 is controlled on the basis of this temperature adjustment method so as to maintain the cell chamber 11 at a constant temperature (40°C).

Figs. 10A and 10B are a plan view and a side view, respectively, of the gas injector 21 for quantitatively injecting a gaseous sample.

The gas injector 21 includes a cylinder 21b disposed on a base 21a, a piston 21c inserted in the cylinder 21c, and a

movable nut 21d connected to the piston 21c, a feed screw 21e threadingly meshed with the nut 21d and a motor 21f for rotating the feed screw 21e which are disposed below the base 21a.

5       The motor 21f is driven for forward and backward rotation by a driving circuit not shown. As the feed screw 21e is rotated by the rotation of the motor 21f, the nut 21d moved forward or backward depending on the rotational direction of the feed screw 21e. The piston 21c advances toward a position  
10 indicated by a dashed line in Fig. 10A. Thus, the gas injector 21 can be flexibly controlled to introduce and extract the gaseous sample in/from the cylinder 21b.

#### IIIa. Measuring procedure 1

      The measuring procedure includes reference gas  
15 measurement, base gas measurement, reference gas measurement, sample gas measurement and reference gas measurement, which are to be performed in this order. Alternatively, base gas measurement, reference gas measurement and base gas measurement, and sample gas measurement, reference gas  
20 measurement and sample gas measurement may be performed in this order. In the latter case, the base gas measurement and the sample gas measurement are each performed twice and, therefore, the operation efficiency is reduced. The former measuring procedure which is more efficient will hereinafter  
25 be described.

During the measurement, the reference gas constantly flows through the reference cell 11c, and the flow rate thereof is always kept constant by the flow meter  $M_1$ .

#### IIIIa-1. Reference measurement

5       As shown in Fig. 11, the clean reference gas is passed through a gas flow path and the cell chamber 11 of the spectrometric apparatus at a rate of 200ml/minute for about 15 seconds for cleaning the gas flow path and the cell chamber 11.

10       In turn, as shown in Fig. 12, the gas flow path is changed, and then the reference gas is passed therethrough for cleaning the gas flow path and the cell chamber 11. After a lapse of about 30 seconds, light intensity are measured by means of the detection elements 25a and 25b.

15       On the basis of the reference measurement, absorbances are calculated.

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}R_1$  and  $^{13}R_1$ , respectively.

#### 20       IIIIa-2. Base gas measurement

The base gas is sucked into the gas injector 21 from the breath sampling bag with the reference gas prevented from flowing through the first and second sample cells 11a and 11b (see Fig. 13).

25       Thereafter, the base gas is mechanically pushed out at a

constant rate (60ml/minute) by the gas injector 21 as shown in Fig. 14 and, at the same time, light intensity are measured by means of the detection elements 25a and 25b.

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}B$  and  $^{13}B$ , respectively.

#### IIIIa-3. Reference measurement

The cleaning of the gas flow path and the cells and the light intensity measurement on the reference gas are performed again (see Figs. 11 and 12).

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}R_2$  and  $^{13}R_2$ , respectively.

#### IIIIa-4. Sample gas measurement

The sample gas is sucked into the gas injector 21 from the breath sampling bag with the reference gas prevented from flowing through the first and second sample cells 11a and 11b (see Fig. 15).

Thereafter, the sample gas is mechanically pushed out at a constant rate (60ml/minute) by the gas injector 21 as shown in Fig. 16 and, at the same time, light intensity are measured by means of the detection elements 25a and 25b.

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}S$  and  $^{13}S$ , respectively.

IIIa-5. Reference measurement

The cleaning of the gas flow path and the cells and the light intensity measurement on the reference gas are performed again (see Figs. 11 and 12).

5       The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}R_3$  and  $^{13}R_3$ , respectively.

IIIb. Measurement procedure 2

10       In the measurement procedure 1, the CO<sub>2</sub> concentrations of the base gas and the sample gas are not adjusted to the same level.

      If the base gas and the sample gas are at the same CO<sub>2</sub> concentration level, the ranges of  $^{12}CO_2$  and  $^{13}CO_2$  calibration curves to be used for determination of the concentrations can  
15       be narrowed. By using limited ranges of the calibration curves, the measurement accuracy can be increased.

      In accordance with the measurement procedure 2, the CO<sub>2</sub> concentrations of the base gas and the sample gas are adjusted to substantially the same level. First, the CO<sub>2</sub>  
20       concentrations of the base gas and the sample gas are measured in a preliminary measurement. If the CO<sub>2</sub> concentration of the base gas obtained in the preliminary measurement is higher than the CO<sub>2</sub> concentration of the sample gas obtained in the preliminary measurement, the base gas is diluted to a CO<sub>2</sub>  
25       concentration level equivalent to that of the sample gas, and



the measurement of the concentration is performed on the base gas and then on the sample gas in a main measurement.

If the CO<sub>2</sub> concentration of the base gas obtained in the preliminary measurement is lower than the CO<sub>2</sub> concentration of the sample gas obtained in the preliminary measurement, the CO<sub>2</sub> concentration of the base gas is measured in the main measurement. The sample gas is diluted to a CO<sub>2</sub> concentration level equivalent to that of the base gas, and then the CO<sub>2</sub> concentration thereof is measured.

The measurement procedure 2 includes preliminary base gas measurement, preliminary sample gas measurement, reference gas measurement, base gas measurement, reference gas measurement, sample gas measurement and reference gas measurement, which are performed in this order.

#### IIb-1. Preliminary base gas measurement

The clean reference gas is passed through the gas flow path and the cell chamber 11 of the spectrometric apparatus for cleaning the gas flow path and the cell chamber 11 and, at the same time, a reference light intensity is measured.

In turn, the base gas is sucked into the gas injector 21 from the breath sampling bag, and then mechanically pushed out at a constant flow rate by means of the gas injector 21. At this time, the intensity of light transmitted through the base gas is measured by means of the detection element 25a to determine an absorbance, and the CO<sub>2</sub> concentration of the base

gas is determined on the basis of the absorbance by using a calibration curve.

#### IIb-2. Preliminary sample gas measurement

5 The clean reference gas is passed through the gas flow path and the cell chamber 11 of the spectrometric apparatus for cleaning the gas flow path and the cell chamber 11 and, at the same time, a reference light intensity is measured.

In turn, the sample gas is sucked into the gas injector 21 from the breath sampling bag, and then mechanically pushed  
10 out at a constant flow rate by means of the gas injector 21. At this time, the intensity of light transmitted through the sample gas is measured by means of the detection element 25a to determine an absorbance, and the CO<sub>2</sub> concentration of the sample gas is determined on the basis of the absorbance by  
15 using the calibration curve.

#### IIb-3. Reference measurement

The gas flow path is changed, and then the reference gas is passed therethrough to clean the gas flow path and the cell chamber 11. After a lapse of about 30 seconds, light intensity  
20 are measured by means of the detection elements 25a and 25b.

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}R_1$  and  $^{13}R_1$ , respectively.

#### IIb-4. Base gas measurement

25 The CO<sub>2</sub> concentration of the base gas obtained by the

first detection element 25a in "IIb-1. Preliminary base gas measurement" is compared with the CO<sub>2</sub> concentration of the sample gas obtained by the first detection element 25a in "IIb-2. Preliminary sample gas measurement". If the CO<sub>2</sub> concentration of the base gas is higher than the CO<sub>2</sub> concentration of the sample gas, the base gas is diluted with the reference gas in the gas injector 21 to a CO<sub>2</sub> concentration level equivalent to that of the sample gas, and then the light intensity measurement is performed on the base gas thus diluted.

Since the CO<sub>2</sub> concentrations of the two breath samples are adjusted to substantially the same level by dilution, the ranges of the <sup>12</sup>CO<sub>2</sub> and <sup>13</sup>CO<sub>2</sub> calibration curves to be used can be narrowed.

It should be noted that the measuring procedure 2 of this embodiment is characterized in that the CO<sub>2</sub> concentrations of the two breath samples are adjusted to substantially the same level, and does not necessarily require to employ a step of maintaining the CO<sub>2</sub> concentration at a constant level as described in JPB 4(1992)-124141. The use of limited ranges of calibration curves can be achieved simply by adjusting the CO<sub>2</sub> concentrations of the base gas and the sample gas to substantially the same level. Since the CO<sub>2</sub> concentrations of the base gas and the sample gas vary within a range of 1% to 5% in actual measurement, it is very troublesome to always

maintain the CO<sub>2</sub> concentrations at a constant level.

If the CO<sub>2</sub> concentration of the base gas is lower than the CO<sub>2</sub> concentration of the sample gas, the base gas is not diluted, and the measurement is performed on the base gas.

5       The base gas is mechanically pushed out at a constant flow rate by the gas injector 21, and light intensity are measured by means of the detection elements 25a and 25b.

10       The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by <sup>12</sup>B and <sup>13</sup>B, respectively.

#### IIb-5. Reference measurement

The cleaning of the gas flow path and the cells and the light intensity measurement on the reference gas are performed again.

15       The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by <sup>12</sup>R<sub>2</sub> and <sup>13</sup>R<sub>2</sub>, respectively.

#### IIb-6. Sample gas measurement

20       If the base gas is diluted in "IIb-4. Base gas measurement", the sample gas is sucked from the breath sampling bag, and then mechanically pushed out at a constant flow rate by the gas injector 21. At this time, light intensity are measured by the detection elements 25a and 25b.

25       If the base gas is not diluted in "IIb-4. Base gas measurement", the sample gas is diluted with the reference gas

to a CO<sub>2</sub> concentration level equivalent to that of the base gas in the gas injector 21, and then the intensity of light transmitted through the sample gas is measured by means of the detection elements 25a and 25b.

5        The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}S$  and  $^{13}S$ , respectively.

#### IIIb-7. Reference measurement

10        The cleaning of the gas flow path and the cells and the light intensity measurement on the reference gas are performed again.

The light intensity thus obtained by the first and second detection elements 25a and 25b are represented by  $^{12}R_3$  and  $^{13}R_3$ , respectively.

#### 15        IV. Data processing

##### IV-1. Calculation of absorbances for base gas

20        Absorbances  $^{12}Abs(B)$  and  $^{13}Abs(B)$  of  $^{12}CO_2$  and  $^{13}CO_2$  in the base gas are calculated on the basis of the transmitted light intensity  $^{12}R_1$ ,  $^{13}R_1$ ,  $^{12}R_2$  and  $^{13}R_2$  for the reference gas and the transmitted light intensity  $^{12}B$  and  $^{13}B$  for the base gas obtained in the measuring procedure 1 or in the measuring procedure 2.

The absorbance  $^{12}Abs(B)$  of  $^{12}CO_2$  is calculated from the following equation:

25        
$$^{12}Abs(B) = -\log[2 \cdot ^{12}B / (^{12}R_1 + ^{12}R_2)]$$

The absorbance  $^{13}\text{Abs}(\text{B})$  of  $^{13}\text{CO}_2$  is calculated from the following equation:

$$^{13}\text{Abs}(\text{B}) = -\log[2 \cdot ^{13}\text{B} / (^{13}\text{R}_1 + ^{13}\text{R}_2)]$$

Since the calculation of the absorbances is based on the  
 5 light intensity obtained in the base gas measurement and the  
 averages  $(^{12}\text{R}_1 + ^{12}\text{R}_2)/2$  and  $(^{13}\text{R}_1 + ^{13}\text{R}_2)/2$  of the light  
 intensity obtained in the reference measurements performed  
 before and after the base gas measurement, the influence of a  
 drift (a time-related influence on the measurement) can be  
 10 eliminated. Therefore, when the apparatus is turned on, there  
 is no need for waiting until the apparatus reaches a thermal  
 equilibrium (it usually takes several hours).

Where the measuring procedure of the base gas  
 measurement, the reference gas measurement and the base gas  
 15 measurement, and the sample gas measurement, the reference gas  
 measurement and the sample gas measurement as describe at the  
 beginning of "IIIa" is employed, the absorbance  $^{12}\text{Abs}(\text{B})$  of  
 $^{12}\text{CO}_2$  in the base gas is calculated from the following  
 equation:

$$^{12}\text{Abs}(\text{B}) = -\log[(^{12}\text{B}_1 + ^{12}\text{B}_2)/2 \cdot ^{12}\text{R}]$$

and the absorbance  $^{13}\text{Abs}(\text{B})$  of  $^{13}\text{CO}_2$  is calculated from the  
 following equation:

$$^{13}\text{Abs}(\text{B}) = -\log[(^{13}\text{B}_1 + ^{13}\text{B}_2)/2 \cdot ^{13}\text{R}]$$

wherein  $^{12}\text{R}$  and  $^{13}\text{R}$  are the transmitted light intensity for the  
 25 reference gas,  $^{12}\text{B}_1$  and  $^{13}\text{B}_1$  are the transmitted light

intensity for the base gas obtained before the reference gas measurement, and  $^{12}B_2$  and  $^{13}B_2$  are the transmitted light intensity for the base gas obtained after the reference gas measurement.

5 IV-2. Calculation of absorbances for sample gas

Absorbances  $^{12}Abs(S)$  and  $^{13}Abs(S)$  of  $^{12}CO_2$  and  $^{13}CO_2$  in the sample gas are calculated on the basis of the transmitted light intensity  $^{12}R_2$ ,  $^{13}R_2$ ,  $^{12}R_3$  and  $^{13}R_3$  for the reference gas and the transmitted light intensity  $^{12}S$  and  $^{13}S$  for the sample gas obtained in the measuring procedure 1 or in the measuring procedure 2.

The absorbance  $^{12}Abs(S)$  of  $^{12}CO_2$  is calculated from the following equation:

$$^{12}Abs(S) = -\log[2 \cdot ^{12}S / (^{12}R_2 + ^{12}R_3)]$$

15 The absorbance  $^{13}Abs(S)$  of  $^{13}CO_2$  is calculated from the following equation:

$$^{13}Abs(S) = -\log[2 \cdot ^{13}S / (^{13}R_2 + ^{13}R_3)]$$

Since the calculation of the absorbances is based on the light intensity obtained in the sample gas measurement and the averages of the light intensity obtained in the reference measurements performed before and after the sample gas measurement, the influence of a drift can be eliminated.

Where the measuring procedure of the base gas measurement, the reference gas measurement and the base gas measurement, and the sample gas measurement, the reference gas

measurement and the sample gas measurement as describe at the beginning of "IIIa" is employed, the absorbance  $^{12}\text{Abs}(\text{S})$  of  $^{12}\text{CO}_2$  in the sample gas is calculated from the following equation:

5 
$$^{12}\text{Abs}(\text{S}) = -\log[(^{12}\text{S}_1 + ^{12}\text{S}_2)/2 \cdot ^{12}\text{R}]$$

and the absorbance  $^{13}\text{Abs}(\text{S})$  of  $^{13}\text{CO}_2$  is calculated from the following equation:

$$^{13}\text{Abs}(\text{S}) = -\log[(^{13}\text{S}_1 + ^{13}\text{S}_2)/2 \cdot ^{13}\text{R}]$$

wherein  $^{12}\text{R}$  and  $^{13}\text{R}$  are the transmitted light intensity for the reference gas,  $^{12}\text{S}_1$  and  $^{13}\text{S}_1$  are the transmitted light intensity for the sample gas obtained before the reference gas measurement, and  $^{12}\text{S}_2$  and  $^{13}\text{S}_2$  are the transmitted light intensity for the sample gas obtained after the reference gas measurement.

15 IV-3. Calculation of concentrations

The  $^{12}\text{CO}_2$  concentration and the  $^{13}\text{CO}_2$  concentration are calculated by using calibration curves.

The calibration curves for  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  are prepared on the basis of measurement performed by using gaseous samples of known  $^{12}\text{CO}_2$  concentrations and gaseous samples of known  $^{13}\text{CO}_2$  concentrations, respectively.

For preparation of the calibration curve for  $^{12}\text{CO}_2$ , the  $^{12}\text{CO}_2$  absorbances for different  $^{12}\text{CO}_2$  concentrations within a range of about 0% to about 6% are measured. The  $^{12}\text{CO}_2$  concentrations and the  $^{12}\text{CO}_2$  absorbances are plotted as



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abscissa and ordinate, respectively, and the curve is determined by the method of least squares. An approximate quadratic curve, which includes relatively small errors, is employed as the calibration curve in this embodiment.

5        For preparation of the calibration curve for  $^{13}\text{CO}_2$ , the  $^{13}\text{CO}_2$  absorbances for different  $^{13}\text{CO}_2$  concentrations within a range of about 0.00% to about 0.07% are measured. The  $^{13}\text{CO}_2$  concentrations and the  $^{13}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, and the curve is  
10       determined by the method of least squares. An approximate quadratic curve, which includes relatively small errors, is employed as the calibration curve in this embodiment.

Strictly speaking, the  $^{13}\text{CO}_2$  absorbance determined by individually measuring gases respectively containing  $^{12}\text{CO}_2$  and  
15        $^{13}\text{CO}_2$  may be different from the  $^{13}\text{CO}_2$  absorbance determined by measuring a gas containing both  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ . This is because the wavelength filters each have a bandwidth and the  $^{12}\text{CO}_2$  absorption spectrum partially overlaps  $^{13}\text{CO}_2$  absorption spectrum. Since gases containing both  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  are to  
20       be measured in this measurement method, the overlap of these spectra should be corrected for preparation of the calibration curves. The calibration curves to be employed in this measurement are subjected to the correction for the overlap of the absorption spectra.

25       For preparation of the calibration curve for the  $^{12}\text{CO}_2$

concentration, the  $^{12}\text{CO}_2$  absorbances for 20 different  $^{12}\text{CO}_2$  concentrations within a range of about 0% to about 6% are measured. The  $^{12}\text{CO}_2$  concentrations and the  $^{12}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, as shown  
5 in Fig. 17A.

The curve, which passes through the respective data points, is determined by the method of least squares. An approximate quadratic curve includes the least error. Therefore, the approximate quadratic curve is employed as the  
10 calibration curve for  $^{12}\text{CO}_2$  in this embodiment.

In turn, five data points are selected which are located around the  $^{12}\text{CO}_2$  concentration of the base gas previously determined on the basis of the calibration curve for  $^{12}\text{CO}_2$ . The five data points fall within a concentration range of  
15 1.5%, which accounts for 25% of the entire concentration range (6%) of the calibration curve shown in Fig. 17A. Then, the data within the limited concentration range are used for the preparation of a new calibration curve (see Fig. 17B). It is confirmed that the preparation of the calibration curve within  
20 the limited data range improves the conformity of the data to the approximate curve, thereby remarkably reducing errors associated with the preparation of the calibration curve. The  $^{12}\text{CO}_2$  concentration of the base gas is determined on the basis of the absorbance  $^{12}\text{Abs(B)}$  of the base gas by using the new  
25 calibration curve for  $^{12}\text{CO}_2$ .

The  $^{12}\text{CO}_2$  concentration of the sample gas is determined in the same manner.

For preparation of the calibration curve for the  $^{13}\text{CO}_2$  concentration, the  $^{13}\text{CO}_2$  absorbances for 20 different  $^{13}\text{CO}_2$  concentrations within a range of about 0.00% to about 0.07% are measured. The  $^{13}\text{CO}_2$  concentrations and the  $^{13}\text{CO}_2$  absorbances are plotted as abscissa and ordinate, respectively, as shown in Fig. 18A.

The curve, which passes through the respective data points, is determined by the method of least squares. An approximate quadratic curve includes the least error. Therefore, the approximate quadratic curve is employed as the calibration curve for  $^{13}\text{CO}_2$  in this embodiment.

In turn, five data points are selected which are located around the  $^{13}\text{CO}_2$  concentration of the base gas previously determined on the basis of the calibration curve for  $^{13}\text{CO}_2$ . The five data points fall within a concentration range of 0.015%, which accounts for about 1/4 of the entire concentration range (0.07%) of the calibration curve shown in Fig. 18A. Then, the data within the limited concentration range are used for the preparation of a new calibration curve (see Fig. 18B). It is confirmed that the preparation of the calibration curve within the limited data range improves the conformity of the data to the approximate curve, thereby remarkably reducing errors associated with the preparation of

the calibration curve. The  $^{13}\text{CO}_2$  concentration of the base gas is determined on the basis of the absorbance  $^{13}\text{Abs}(\text{B})$  of the base gas by using the new calibration curve for  $^{13}\text{CO}_2$ .

5 The  $^{13}\text{CO}_2$  concentration of the sample gas is determined in the same manner.

The  $^{12}\text{CO}_2$  concentration and  $^{13}\text{CO}_2$  concentration of the base gas are represented by  $^{12}\text{Conc}(\text{B})$  and  $^{13}\text{Conc}(\text{B})$ , respectively. The  $^{12}\text{CO}_2$  concentration and  $^{13}\text{CO}_2$  concentration of the sample gas are represented by  $^{12}\text{Conc}(\text{S})$  and  $^{13}\text{Conc}(\text{S})$ ,  
10 respectively.

#### IV-4. Calculation of concentration ratios

The concentration ratio of  $^{13}\text{CO}_2$  to  $^{12}\text{CO}_2$  is determined. The concentration ratios in the base gas and in the sample gas are expressed as  $^{13}\text{Conc}(\text{B})/^{12}\text{Conc}(\text{B})$  and  $^{13}\text{Conc}(\text{S})/^{12}\text{Conc}(\text{S})$ ,  
15 respectively.

Alternatively, the concentration ratios in the base gas and in the sample gas may be defined as  $^{13}\text{Conc}(\text{B})/^{12}\text{Conc}(\text{B})+^{13}\text{Conc}(\text{B})$  and  $^{13}\text{Conc}(\text{S})/^{12}\text{Conc}(\text{S})+^{13}\text{Conc}(\text{S})$ , respectively. Since the  $^{12}\text{CO}_2$  concentration is much higher  
20 than the  $^{13}\text{CO}_2$  concentration, the concentration ratios expressed in the former way and in the latter way are substantially the same.

#### IV-5a. Correction of concentration ratios

As described in "BACKGROUND ART", the concentration  
25 ratios obtained in the aforesaid manner deviate from actual

concentrations, depending on the  $^{12}\text{CO}_2$  concentration.

Although the cause of the deviation has not been elucidated yet, the deviation supposedly results from changes in the spectroscopic characteristics such as reflectance, refractive index and stray light in dependence on the  $^{12}\text{CO}_2$  concentration and from the error characteristics of the least square method employed for preparation of the calibration curves.

If the concentration ratio is determined without correcting the deviation, a critical error may result. Therefore, absorbances  $^{12}\text{Abs}$  and  $^{13}\text{Abs}$  of  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  in gaseous samples having the same concentration ratio but different  $^{12}\text{CO}_2$  concentrations are measured, and the  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  concentrations and  $^{13}\text{CO}_2$  concentration ratios of the gaseous samples are determined by using the calibration curves. Then, the  $^{12}\text{CO}_2$  concentrations  $^{12}\text{Conc}$  and the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  are plotted as abscissa and ordinate, respectively.

The result is shown in Fig. 1.

The concentration ratios plotted as ordinate in the graph of Fig.1 are not normalized. The concentration ratios may be normalized for easy processing of data. Fig. 19 illustrates a graph obtained by way of standardization of the concentration ratios in which a concentration ratio in a gaseous sample of the lowest  $\text{CO}_2$  concentration is regarded as

"1". (The concentration ratios thus normalized are hereinafter referred to as "normalized concentration ratios".)

To obtain an approximate curve accommodating these plotted data, the method of least squares is employed for approximation of the data. It is experientially known that a function of the fourth degree expressed by the following equation (1) provides the most accurate approximate curve.

$$F(x) = ax^4 + bx^3 + cx^2 + dx + e \dots (1)$$

wherein F is a normalized concentration ratio, a to d are coefficients, e is a constant, and x is a  $^{12}\text{CO}_2$  concentration. Therefore, the fourth-order function (1) is used as a correction equation. Alternatively, a spline function may be used.

Standardized  $^{13}\text{CO}_2/^{12}\text{CO}_2$  concentration ratios are calculated from the correction equation (1) on the basis of the  $^{12}\text{CO}_2$  concentrations  $^{12}\text{Conc(B)}$  and  $^{12}\text{Conc(S)}$  in the breath samples of the patient. Then, the concentration ratios  $^{13}\text{Conc(B)}/^{12}\text{Conc(B)}$  and  $^{13}\text{Conc(S)}/^{12}\text{Conc(S)}$  of the base gas and the sample gas obtained in the measurement are respectively divided by the normalized concentration ratios calculated from the correction equation (1). Thus, corrected concentration ratios are obtained as follows:

Corrected concentration ratio

$$= ^{13}\text{Conc(B)} / [ ^{12}\text{Conc(B)} \cdot F(^{12}\text{Conc(B)}) ]$$

Corrected concentration ratio

$$= {}^{13}\text{Conc}(\text{S}) / [{}^{12}\text{Conc}(\text{S}) \cdot F({}^{12}\text{Conc}(\text{S}))]$$

#### IV-5b. Correction of concentration ratios

5 The  ${}^{13}\text{CO}_2$  concentration ratios of the base gas and the sample gas are subjected to a correction for oxygen concentration according to the present invention.

The  ${}^{13}\text{CO}_2$  concentration ratios are corrected by using a graph (Fig. 2) in which measurements of the  ${}^{13}\text{CO}_2$  concentration ratio are plotted with respect to the oxygen contents of gaseous samples.

More specifically, normalized  ${}^{13}\text{CO}_2$  concentration ratios are obtained from the graph shown in Fig. 2 on the basis of the concentrations of oxygen in the breath samples which are measured by means of the  $\text{O}_2$  sensor. Then, the  ${}^{13}\text{CO}_2$  concentration ratios of the base gas and the sample gas are respectively divided by the normalized  ${}^{13}\text{CO}_2$  concentration ratios. Thus, the  ${}^{13}\text{CO}_2$  concentration ratios corrected depending on the oxygen concentrations can be obtained.

#### IV-6. Determination of change in ${}^{13}\text{C}$

20 A difference in  ${}^{13}\text{C}$  between the sample gas and the base gas is calculated from the following equation:

$$\Delta {}^{13}\text{C} = [\text{Concentration ratio of sample gas} - \text{Concentration ratio of base gas}] \times 10^3 / [\text{Concentration ratio of base gas}]$$

(Unit: per mill)

#### 25 V. Modification

The present invention is not limited to the embodiment described above. In the above-mentioned embodiment, the  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  concentrations of the base gas and the sample gas are determined, then the concentration ratios thereof are calculated, and the concentration ratios are subjected to the oxygen concentration correction. Alternatively, the concentration ratios may be determined after the  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  concentrations of the base gas and the sample gas are determined and the  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  concentrations are corrected by way of the oxygen concentration correction.

## VI. Experiments

### VI-1.

The absorbances of gaseous samples respectively containing  $^{12}\text{CO}_2$  in concentrations  $^{12}\text{Conc}$  of 1%, 2%, 3%, 4%, 5% and 6% with a concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$  of 1.077% were measured in accordance with the method for spectrometrically measuring an isotopic gas. The  $^{12}\text{CO}_2$  concentrations  $^{12}\text{Conc}$  and  $^{13}\text{CO}_2$  concentrations  $^{13}\text{Conc}$  of the gaseous samples were determined on the basis of the measured absorbances by using the calibration curves. The  $^{12}\text{CO}_2$  concentrations  $^{12}\text{Conc}$  and the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were plotted as abscissa and ordinate, respectively, as shown in Fig. 20.

The maximum and minimum values of the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were 1.083% and 1.076%, respectively, and



the difference therebetween was 0.007%.

In turn, the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were corrected by using the correction equation (1), thus providing a less undulant curve as shown in Fig. 21. In Fig. 21, the maximum and minimum values of the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were 1.078% and 1.076%, respectively, and the difference therebetween was 0.0015%.

Therefore, the correction with the correction equation (1) remarkably reduced the variation in the concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$ .

#### VI-2.

The absorbances of gaseous samples respectively containing  $^{12}\text{CO}_2$  in concentrations  $^{12}\text{Conc}$  of 1%, 2%, 3%, 4%, 5% and 6% with a concentration ratio  $^{13}\text{Conc}/^{12}\text{Conc}$  of 1.065% were measured in accordance with the method for spectrometrically measuring an isotopic gas. The  $^{12}\text{Conc}$  and the  $^{13}\text{Conc}$  were determined on the basis of the measured absorbances by using the calibration curves shown in Figs. 17A and 18A. The  $^{12}\text{CO}_2$  concentrations  $^{12}\text{Conc}$  and the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were plotted as abscissa and ordinate, respectively, as shown in Fig. 22.

The maximum and minimum values of the concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were 1.077% and 1.057%, respectively, and the difference therebetween was 0.02%.

In turn, concentration ratios  $^{13}\text{Conc}/^{12}\text{Conc}$  were

determined by using the calibration curves shown in Figs. 17A and 18A and then using the limited-range calibration curves shown in Figs. 17B and 18B, thus providing a less undulant curve as shown in Fig. 23. In Fig. 23, the maximum and  
5 minimum values of the concentration ratios  $^{13}\text{C}_{\text{Conc}}/^{12}\text{C}_{\text{Conc}}$  were 1.066% and 1.064%, respectively, and the difference therebetween was 0.002%.

Therefore, the method of the present invention, in which the calibration curves were produced again, remarkably reduced  
10 the variation in the concentration ratio  $^{13}\text{C}_{\text{Conc}}/^{12}\text{C}_{\text{Conc}}$ .

#### VI-3.

The absorbances of gaseous samples having different known  $^{13}\text{CO}_2$  concentration ratios and containing various concentration of oxygen (up to 90%) were measured, and then  
15 the  $^{13}\text{CO}_2$  concentration ratios were determined on the basis of the measured absorbances by using the calibration curves. Further, the  $^{13}\text{CO}_2$  concentration ratios thus determined were corrected by using a correction line as shown in Fig. 2.

The actual  $^{13}\text{CO}_2$  concentration ratios and the  $^{13}\text{CO}_2$   
20 concentration ratios thus corrected were normalized, and plotted as abscissa and ordinate, respectively, as shown in Fig. 24.

In Fig. 24, the relationship between the actual  $^{13}\text{CO}_2$  concentration ratio and the measured  $^{13}\text{CO}_2$  concentration ratio  
25 is about 1:1 (or the slope of the fitting curve in Fig. 24 is

about 1). In comparison with the prior art shown in Fig. 4, in which the relationship between the actual  $^{13}\text{CO}_2$  concentration ratio and the measured  $^{13}\text{CO}_2$  concentration ratio is about 1:0.3 (or the slope of the fitting curve is about 0.3), the measurement accuracy was drastically improved by performing the correction.

Thus, the correction using the correction line remarkably improved the accuracy of the measurement of the  $^{13}\text{CO}_2$  concentration ratio.

#### VI-4.

The  $^{12}\text{CO}_2$  concentration of the same sample gas containing carbon dioxide was measured a plurality of times by means of the apparatus for spectrometrically measuring an isotopic gas.

After one hour warming-up of apparatus, a measuring procedure consisting of the reference gas measurement, the sample gas measurement, the reference gas measurement, the sample gas measurement and the reference gas measurement were performed ten times on the same sample gas. The  $^{12}\text{CO}_2$  concentration was determined in each cycle of the measuring procedure in accordance with the method A of the present invention in which the absorbance of  $^{12}\text{CO}_2$  in the sample gas was determined on the basis of an average of values obtained in the reference gas measurements performed before and after the sample gas measurement, and in accordance with the prior art method B in which the absorbance of  $^{12}\text{CO}_2$  in the sample

gas was determined on the basis of a value obtained in the reference measurement only before the sample gas measurement.

The results of the calculation of the concentrations in accordance with the method A are shown in Table 1. In Table 1, the concentrations obtained in the second and subsequent measurements were normalized by regarding a concentration obtained in the first measurement as "1". The standard deviation of the concentration data calculated in accordance with the method A was 0.0009.

Table 1

1	2	3	4	5
1	1.0011	0.9996	0.9998	1.0011
6	7	8	9	10
0.9982	1	1.0014	1.0005	1.0006

Table 2

1	2	3	4	5
1	1.0024	1.0001	0.9996	1.0018

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6	7	8	9	10
0.9986	1	1.0022	1.0014	1.0015

As can be understood from the foregoing, the method of  
the present invention, in which the absorbances are determined  
on the basis of the light intensity measured on the sample gas  
and an average of the light intensity measured on the reference  
gas, provides concentration data with little variation.

**Claims:**

1. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing a plurality of component gases into a cell,  
5 measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases, and processing data of the light intensity to determine concentrations of the component gases in the gaseous test sample, the method characterized by: a first step of  
10 introducing the gaseous test sample into the cell and measuring absorbances of the respective component gases in the gaseous test sample; a second step of determining concentrations and concentration ratios of the component gases in the gaseous test sample on the basis of calibration curves;  
15 and a third step of obtaining concentration ratio correction values for the component gases on the basis of the concentrations of the component gases obtained in the second step by using correction curves preliminary prepared by measuring absorbances of the component gases in gaseous  
20 samples containing the respective component gases in known concentrations with known concentration ratios, determining concentrations and concentration ratios of the component gases in the gaseous samples on the basis of the calibration curves, and by plotting the thus determined concentrations and  
25 concentration ratios of the component gases in the gaseous

samples, and respectively dividing the concentration ratios of the component gases obtained in the second step by the concentration ratio correction values for the component gases, thereby correcting the concentration ratios of the component gases in the gaseous test sample.

2. A method as set forth in claim 1, wherein the correction curves prepared in the third step are approximate fourth-order curves respectively representing the relationships between the concentrations and concentration ratios of the component gases in the gaseous samples determined in the third step.

3. A method as set forth in claim 1, wherein the plurality of component gases include  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ .

4. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing a plurality of component gases into a cell, measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases, and processing data of the light intensity to determine concentrations of the component gases in the gaseous test sample, the method characterized by: a first step of introducing the gaseous test sample into the cell and measuring absorbances of the respective component gases in the

gaseous test sample; a second step of tentatively determining concentrations of the component gases in the gaseous test sample on the basis of calibration curves prepared by using data obtained by measuring gaseous samples respectively  
5 containing the component gases in known concentrations within a predetermined range; and a third step of preparing new calibration curves by using some of the data within limited ranges around the concentrations of the component gases in the gaseous test sample tentatively determined in the second step,  
10 and determining concentrations of the component gases in the gaseous test sample by using the calibration curves thus prepared.

5. A method as set forth in claim 4, wherein the plurality  
15 of component gases include  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ .

6. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing  $^{13}\text{CO}_2$  into a cell, measuring an intensity of light  
20 transmitted through the gaseous test sample at a wavelength suitable for  $^{13}\text{CO}_2$ , and processing data of the light intensity to determine a concentration of  $^{13}\text{CO}_2$  in the gaseous test sample, the method characterized by: a first step of introducing the gaseous test sample into the cell and  
25 measuring an absorbance of  $^{13}\text{CO}_2$  in the gaseous test sample; a



second step of determining a concentration of  $^{13}\text{CO}_2$  in the gaseous test sample on the basis of a calibration curve; and a third step of measuring an oxygen concentration in the gaseous test sample, obtaining a concentration correction value for  $^{13}\text{CO}_2$  on the basis of a correction curve and the measured oxygen concentration, said correction curve being preliminary prepared by measuring absorbances of  $^{13}\text{CO}_2$  in gaseous samples containing  $^{13}\text{CO}_2$  and oxygen in known concentrations, determining concentrations of  $^{13}\text{CO}_2$  in the gaseous samples on the basis of the calibration curve, and by plotting the concentrations of  $^{13}\text{CO}_2$  thus determined with respect to the oxygen concentrations, and dividing the concentration of  $^{13}\text{CO}_2$  obtained in the second step by the concentration correction value for  $^{13}\text{CO}_2$  determined on the basis of the correction curve, thereby correcting the concentration of  $^{13}\text{CO}_2$  in the gaseous test sample.

7. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  into a cell, measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ , and processing data of the light intensity to determine concentrations of or a concentration ratio between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  in the gaseous test sample, the method characterized by: a first step of

introducing the gaseous test sample into the cell and measuring absorbances of  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  in the gaseous test sample; a second step of determining concentrations of or a concentration ratio between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  in the gaseous test sample on the basis of calibration curves; and a third step of measuring an oxygen concentration in the gaseous test sample, obtaining concentration correction values or a concentration ratio correction value for  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  on the basis of correction curves and the measured oxygen concentration, said correction curves being preliminary prepared by measuring absorbances of  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  in gaseous samples containing  $^{12}\text{CO}_2$ ,  $^{13}\text{CO}_2$  and oxygen in known concentrations, determining concentrations of or concentration ratios between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  in the gaseous samples on the basis of the calibration curves, and by plotting the concentrations of or the concentration ratios between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  thus determined with respect to the oxygen concentrations, and respectively dividing the concentrations of or the concentration ratio between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  determined in the second step by the concentration correction values or the concentration ratio correction value determined on the basis of the correction curves, thereby correcting the concentrations of or the concentration ratio between  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  in the gaseous test sample.

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8. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing a plurality of component gases into a cell, measuring absorbances of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases, and determining concentrations of the respective component gases on the basis of calibration curves prepared by measuring gaseous samples respectively containing the component gases in known concentrations, the method characterized in that a reference gas measurement in which a light intensity is measured with a reference gas filled in the cell and a sample measurement in which a light intensity is measured with the gaseous test sample filled in the cell are alternately performed; and the absorbances are determined on the basis of the light intensity obtained in the sample measurement and an average of light intensity obtained in the reference gas measurements performed before and after the sample measurement.

9. A method as set forth in claim 8, wherein the plurality of component gases include  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ .

10. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing a plurality of component gases into a cell,

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measuring absorbances of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases and determining concentrations of the respective component gases on the basis of calibration curves prepared by measuring gaseous samples respectively containing the component gases in known concentrations, the method characterized in that a reference gas measurement in which a light intensity is measured with a reference gas filled in the cell and a sample measurement in which a light intensity is measured with the gaseous test sample filled in the cell are alternately performed, and the absorbances are determined on the basis of the light intensity obtained in the reference gas measurement and an average of light intensity obtained in the sample measurements performed before and after the reference gas measurement.

11. A method as set forth in claim 10, wherein the plurality of component gases include  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$ .

12. A method for spectrometrically measuring an isotopic gas, comprising the steps of introducing a gaseous test sample containing  $^{12}\text{CO}_2$  and  $^{13}\text{CO}_2$  as component gases into a cell, measuring absorbances of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases, and determining concentrations of the

respective component gases on the basis of calibration curves prepared by measuring gaseous samples respectively containing the component gases in known concentrations, the method characterized in that two gaseous test samples obtained from one body are measured and, if a concentration of  $^{12}\text{CO}_2$  in one of the two gaseous test samples is higher than a concentration of  $^{12}\text{CO}_2$  in the other gaseous test sample, said one gaseous test sample is diluted to a  $^{12}\text{CO}_2$  concentration level equivalent to that of the other gaseous test sample, and then  $^{13}\text{CO}_2/^{12}\text{CO}_2$  concentration ratios in the respective gaseous test samples are determined.

13. A method as set forth in claim 12, further characterized by a preliminary measurement and a main measurement, wherein concentrations of  $\text{CO}_2$  in first and second gaseous test samples obtained from one body are respectively measured in the preliminary measurement and, if the measured concentration of  $\text{CO}_2$  in the first gaseous test sample is higher than the measured concentration of  $\text{CO}_2$  in the second gaseous test sample, the first gaseous test sample is diluted to a  $\text{CO}_2$  concentration level equivalent to that of the second gaseous test sample, then a  $^{13}\text{CO}_2/^{12}\text{CO}_2$  concentration ratio in the first gaseous test sample thus diluted is determined and a  $^{13}\text{CO}_2/^{12}\text{CO}_2$  concentration ratio in the second gaseous test sample is determined in the main measurement.

14. A method as set forth in claim 12, further characterized by a preliminary measurement and a main measurement, wherein concentrations of CO<sub>2</sub> in first and second gaseous test samples obtained from one body are respectively measured in the preliminary measurement, and if the measured concentration of CO<sub>2</sub> in the first gaseous test sample is lower than the measured concentration of CO<sub>2</sub> in the second gaseous test sample, a <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio in the first gaseous test sample is determined, then the second gaseous test sample is diluted to a CO<sub>2</sub> concentration level equivalent to that of the first gaseous test sample, and a <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio in the second gaseous test sample thus diluted is determined in the main measurement.
15. An apparatus for spectrometrically measuring an isotopic gas, which is adapted to determine concentrations of a plurality of component gases in a gaseous test sample by introducing the gaseous test sample into a cell, then measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases, and processing data of the light intensity, characterized by gas injection means for sucking therein the gaseous test sample and then injecting the gaseous test sample into the cell by mechanically pushing out the gaseous test sample at a constant rate.

16. An apparatus as set forth in claim 15, further characterized by temperature maintaining means for maintaining the cell receiving the gaseous test sample introduced therein at a constant temperature.

5

17. An apparatus for spectrometrically measuring an isotopic gas, which is adapted to determine concentrations of a plurality of component gases in a gaseous test sample by introducing the gaseous test sample into a cell, then

10

measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for the respective component gases and processing data of the light intensity, characterized in that the cell receiving the gaseous test sample introduced therein is positioned in the light path between a light source and a photoreceptor, and a reference cell filled with a reference gas having no absorption at the wavelengths for measurement is disposed in a portion of the light path not occupied by the cell.

15

20

18. An apparatus as set forth in claim 17, further characterized by gas flow generating means for constantly passing the reference gas through the reference cell at a constant flow rate.

19. An apparatus as set forth in claim 17, further

25

characterized by temperature maintaining means for maintaining

the cell receiving the gaseous test sample introduced therein and the reference cell at a constant temperature.

20. An apparatus for spectrometrically measuring an isotopic  
5 gas, which is adapted to determine concentrations of a plurality of component gases in a gaseous test sample by introducing the gaseous test sample into two cells, then measuring intensity of light transmitted through the gaseous test sample at wavelengths suitable for the respective  
10 component gases and processing data of the light intensity, characterized in that the two cells for receiving the gaseous test sample introduced therein are disposed along light paths between a light source and a photoreceptor and have different lengths, and a reference cell filled with a reference gas  
15 having no absorption at the wavelengths for measurement is disposed between a shorter one of the two cells and the photoreceptor or between the light source and the shorter cell.

20 21. An apparatus as set forth in claim 20, further characterized by gas flow generating means for constantly passing the reference gas through the reference cell at a constant flow rate.

22. An apparatus as set forth in claim 20, further  
25 characterized by temperature maintaining means for maintaining



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the cells receiving the gaseous test sample introduced therein and the reference cell at a constant temperature.

23. A breath sampling bag, comprising a plurality of breath  
5 accumulating chambers joined together for respectively  
accumulating a plurality of breath samples and a plurality of  
breath introduction pipes to be respectively connected to a  
plurality of breath inlets of a gas measuring apparatus for  
breath measurement to introduce the breath samples from the  
10 respective breath accumulating chambers into the gas measuring  
apparatus, and characterized in that the breath introduction  
pipes are each configured such that the breath introduction  
pipes are prevented from being connected to wrong breath  
inlets of the gas measuring apparatus.

15  
24. A gas measuring apparatus, which is adapted to measure a  
plurality of breath samples accumulated in a breath sampling  
bag comprising a plurality of breath accumulating chambers  
joined together and a plurality of breath introduction pipes  
20 through which the breath samples are respectively introduced  
from a living body into the plurality of breath accumulating  
chambers, comprising a plurality of breath inlets for  
introducing the breath samples from the breath accumulating  
chambers through the breath introduction pipes, and  
25 characterized in that the breath inlets are each configured

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such that the breath inlets are prevented from being connected to wrong breath introduction pipes.

25. A breath sampling bag, comprising a breath accumulating  
5 chamber for accumulating breath and a breath introduction pipe  
for introducing the breath from a living body into the breath  
accumulating chamber, and characterized in that the breath  
introduction pipe has resistance generating means for  
generating a resistance to the blowing of the breath during  
10 sampling of the breath.

26. A breath sampling bag, comprising a breath accumulating  
chamber for accumulating breath and a breath introduction pipe  
for introducing the breath from a living body into the breath  
15 accumulating chamber, and characterized in that the breath  
introduction pipe has a detachable filter for removing  
moisture from the breath during sampling of the breath.

27. A breath sampling bag, comprising a breath accumulating  
20 chamber for accumulating breath and a breath introduction pipe  
for introducing the breath from a living body into the breath  
accumulating chamber, and characterized in that the breath  
introduction pipe has a valve for preventing the back flow of  
the sampled breath.

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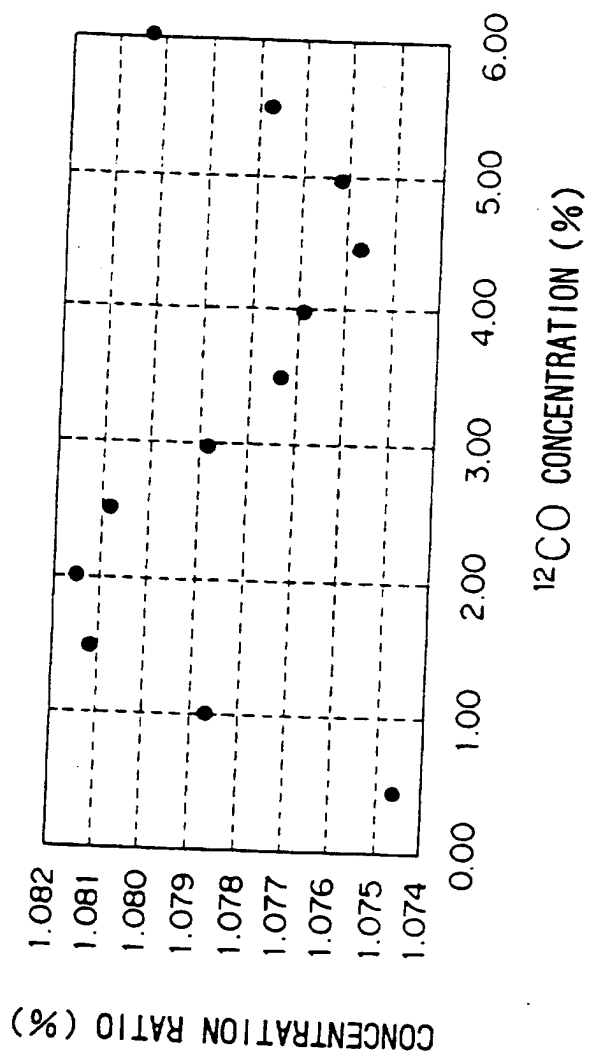
28. A gas measuring apparatus, which is adapted to measure a breath sample accumulated in a breath sampling bag comprising a breath accumulating chamber and a breath introduction pipe with a back-flow prevention valve through which the breath sample is introduced from a living body into the breath accumulating chamber, comprising a breath inlet for introducing the breath sample from the breath sampling bag through the breath introduction pipe, and characterized in that the breath inlet has means for disabling the function of the valve when the breath introduction pipe is connected to the breath inlet.

15

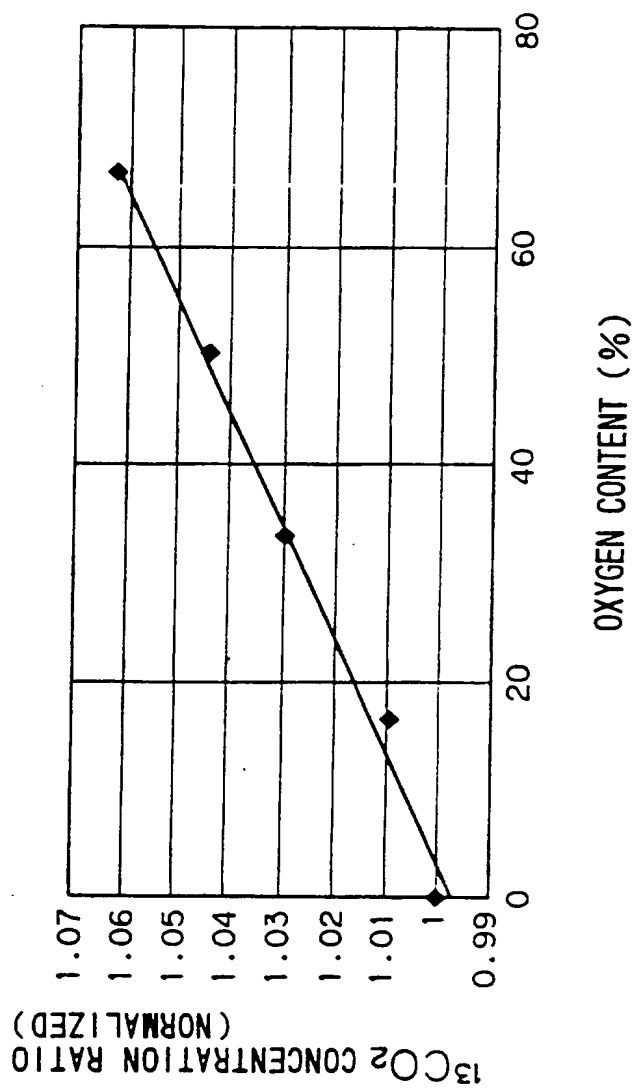
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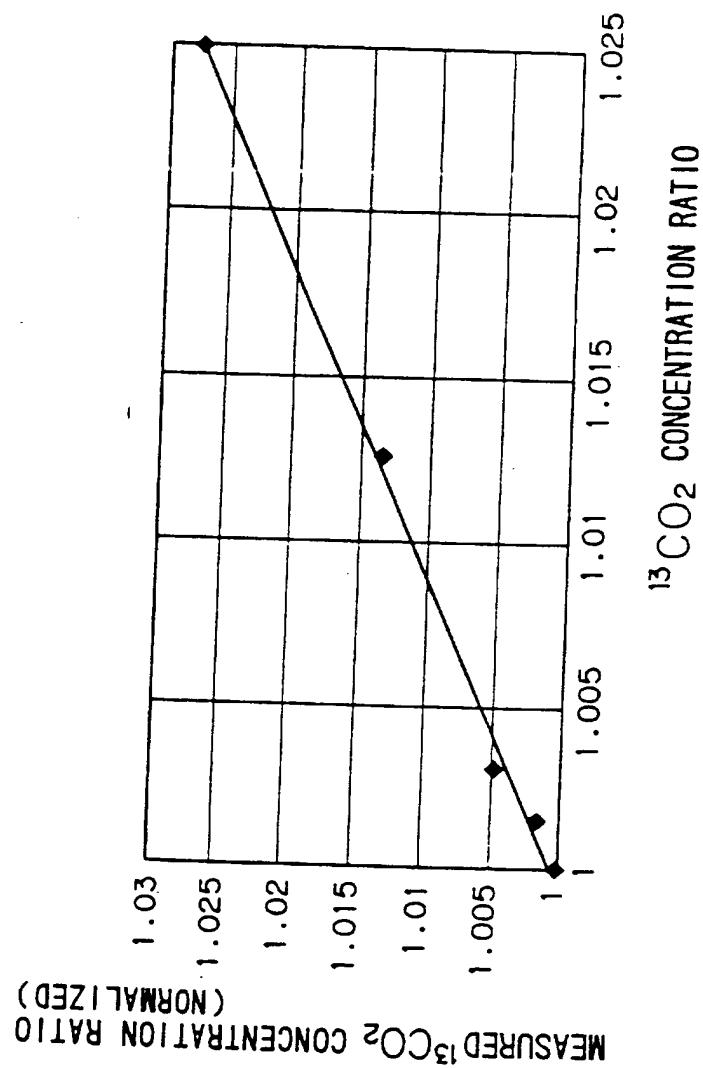
1/24

FIG. 1  
(PRIOR ART)

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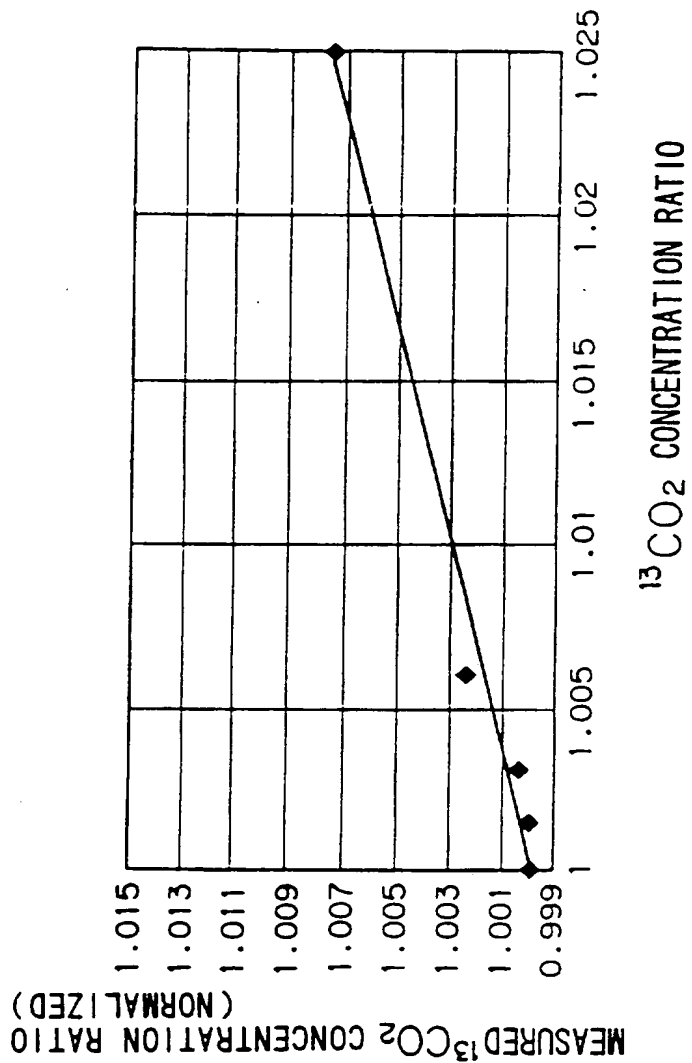
FIG. 2  
(PRIOR ART)

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FIG. 3  
(PRIOR ART)

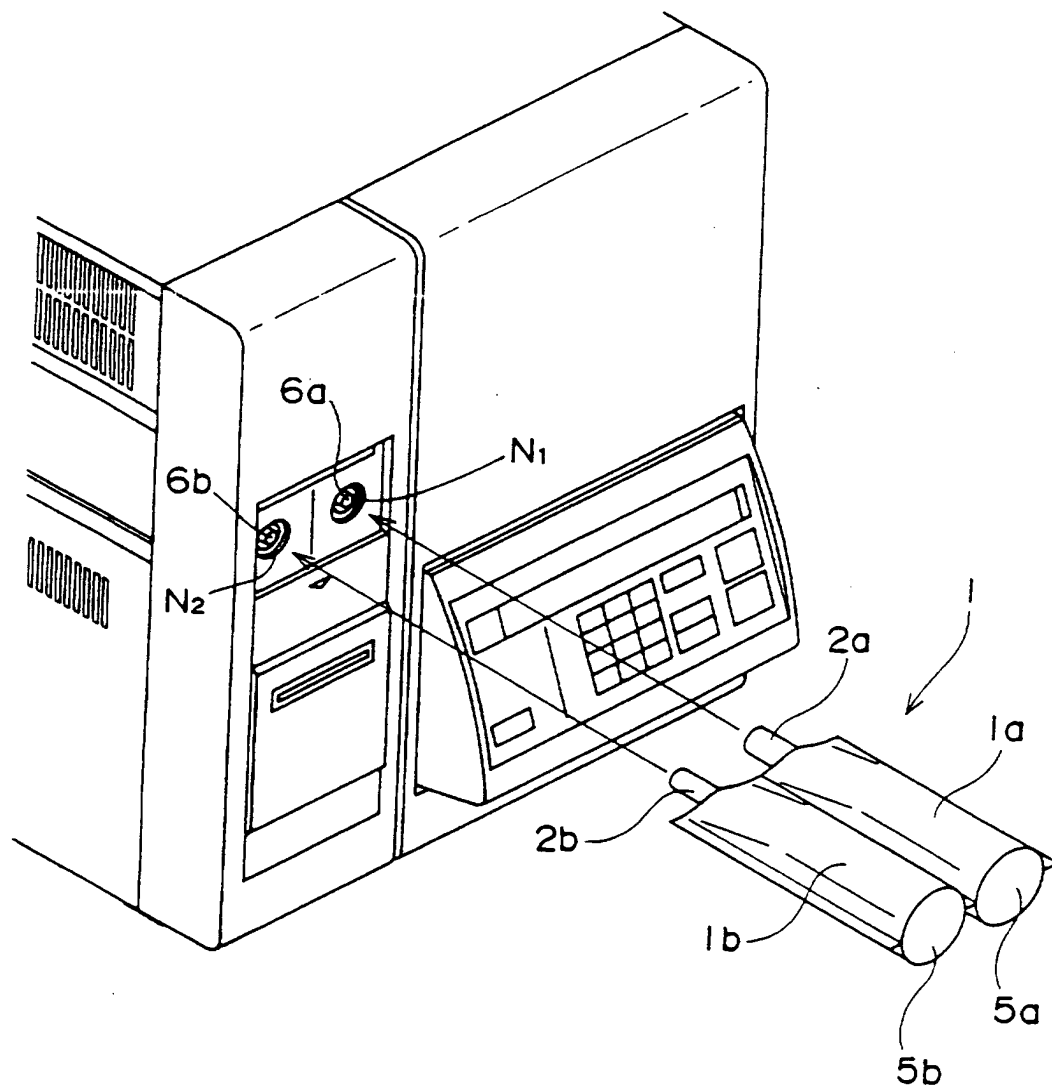
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FIG. 4  
(PRIOR ART)



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FIG. 5

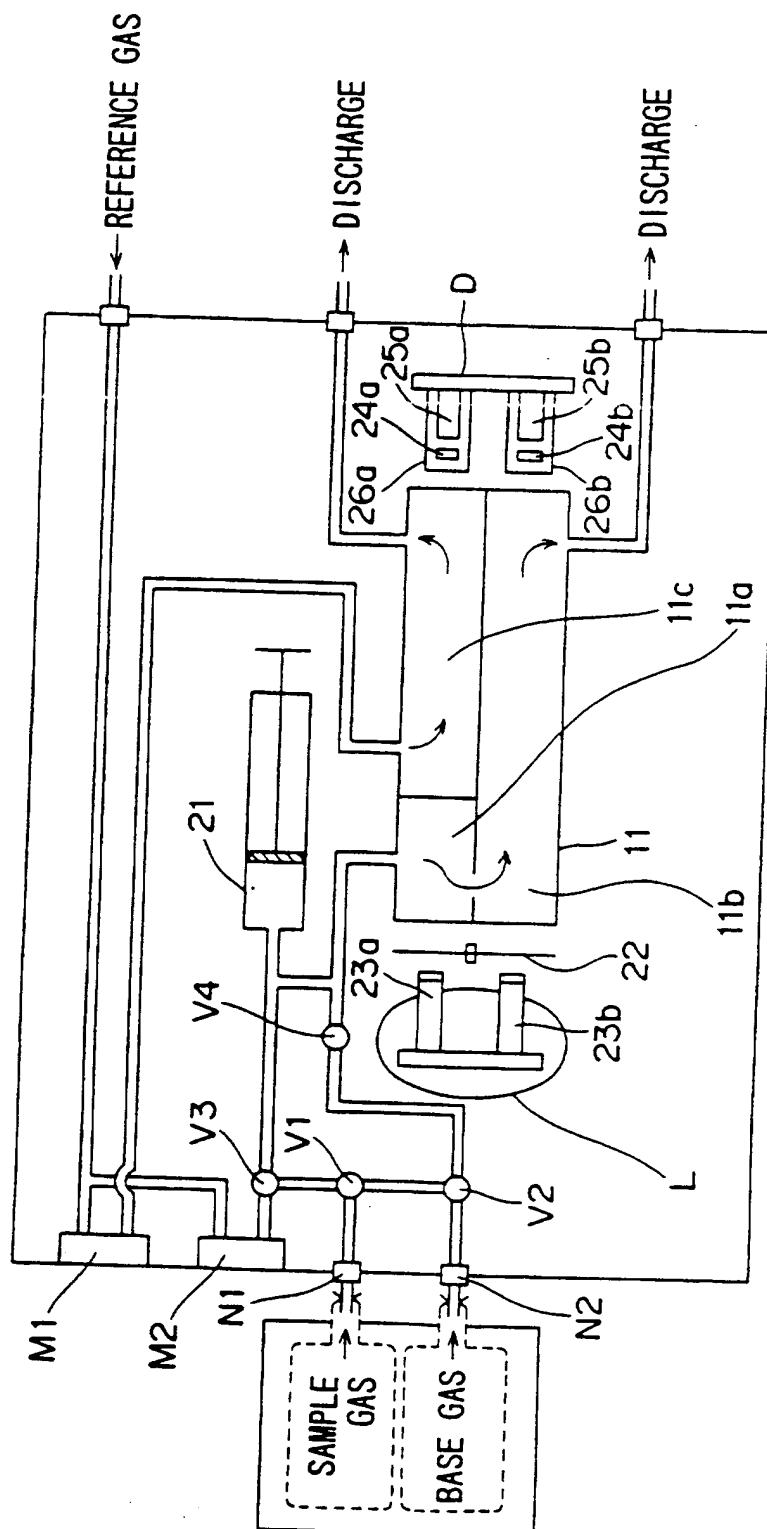






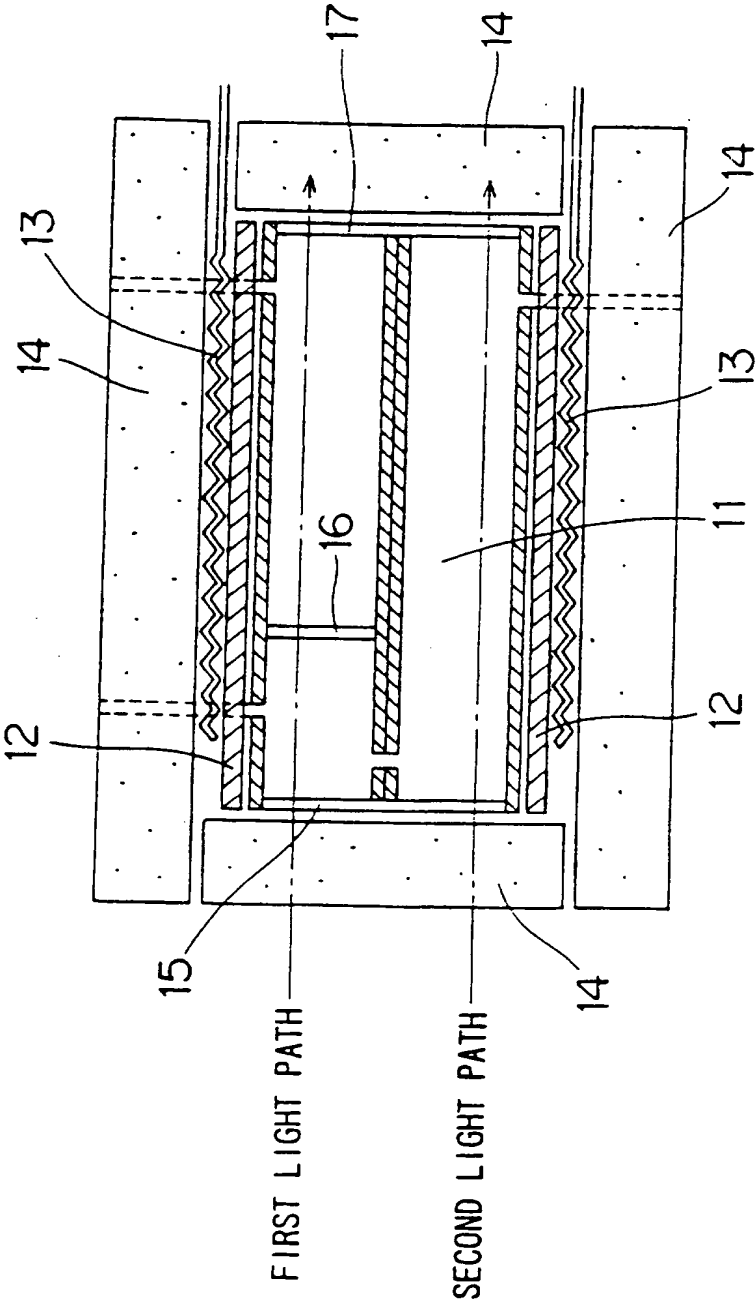
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FIG. 7



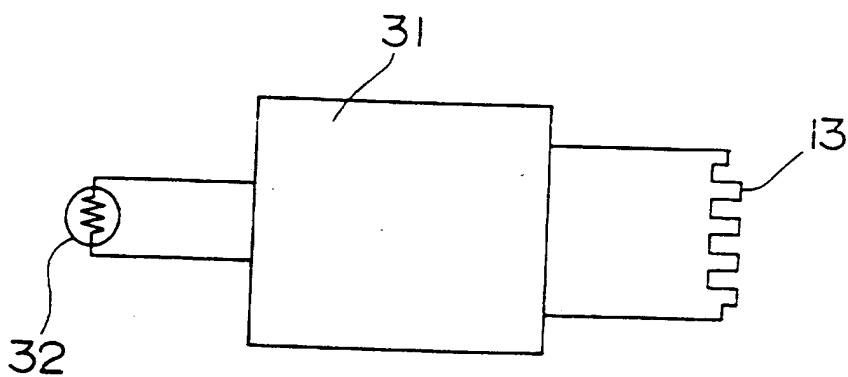
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FIG. 8



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FIG. 9



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FIG. 10A

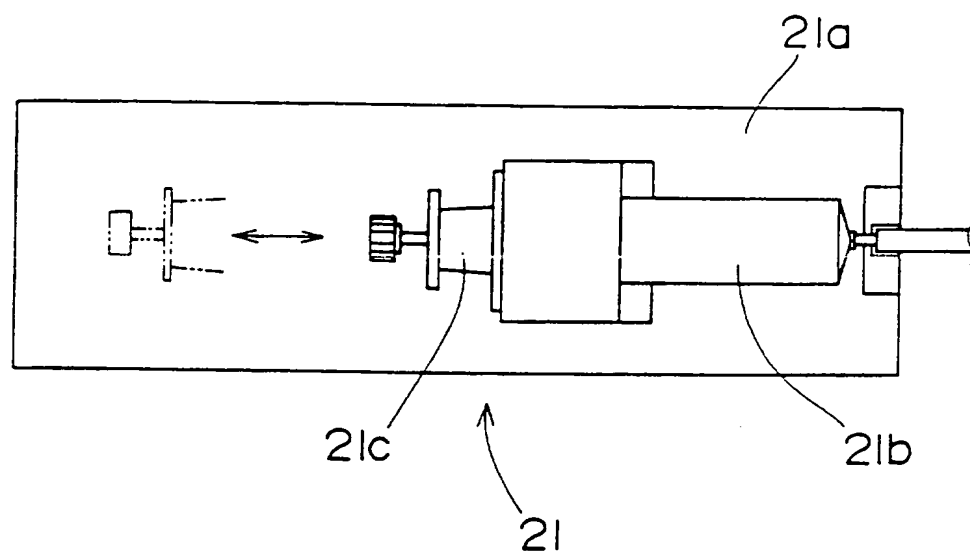
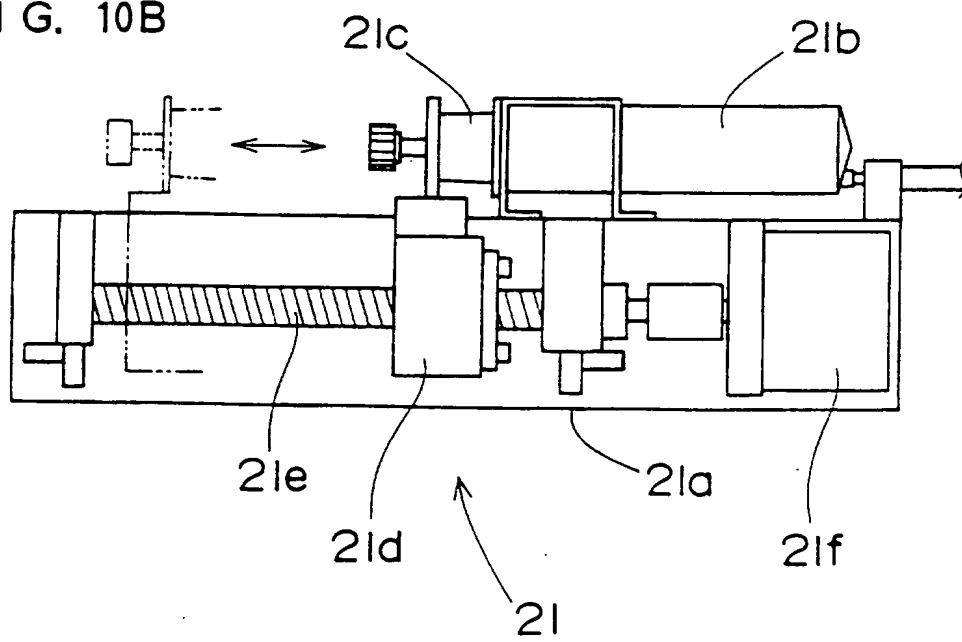
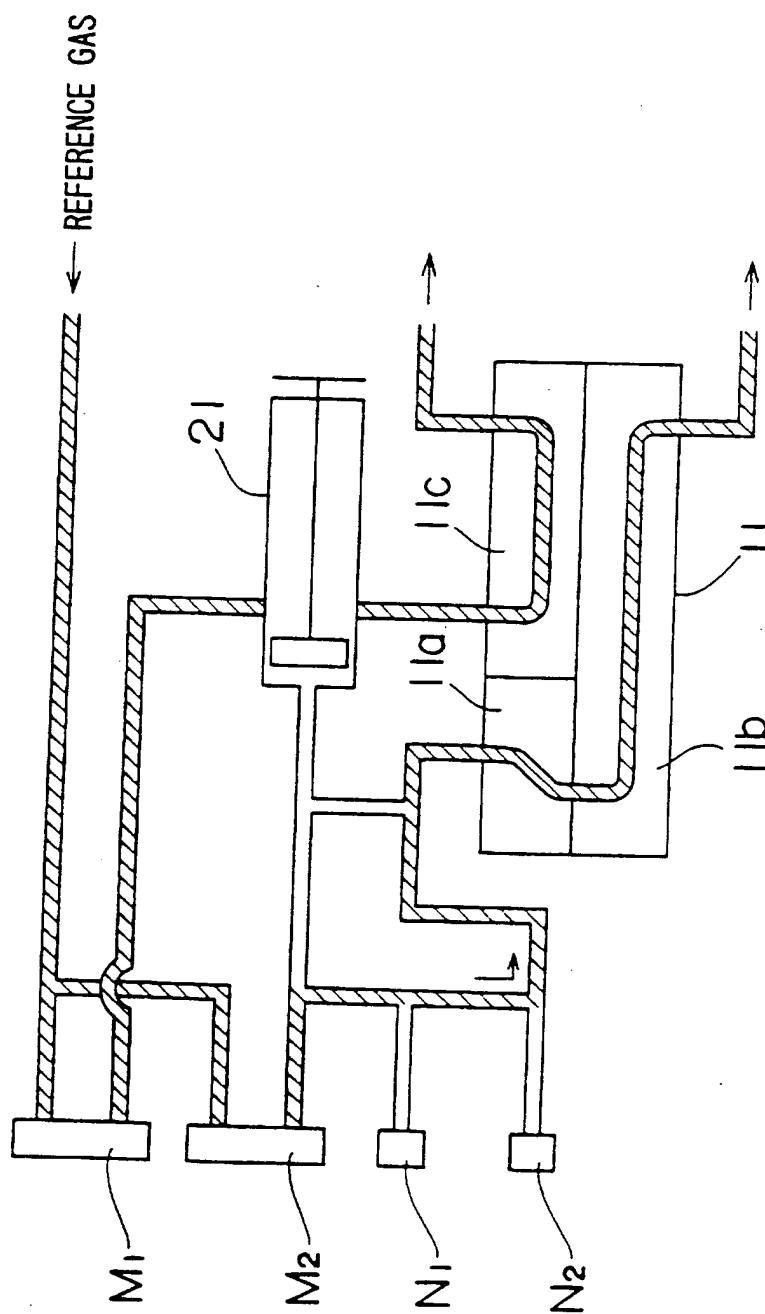


FIG. 10B



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FIG. 11



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FIG. 12

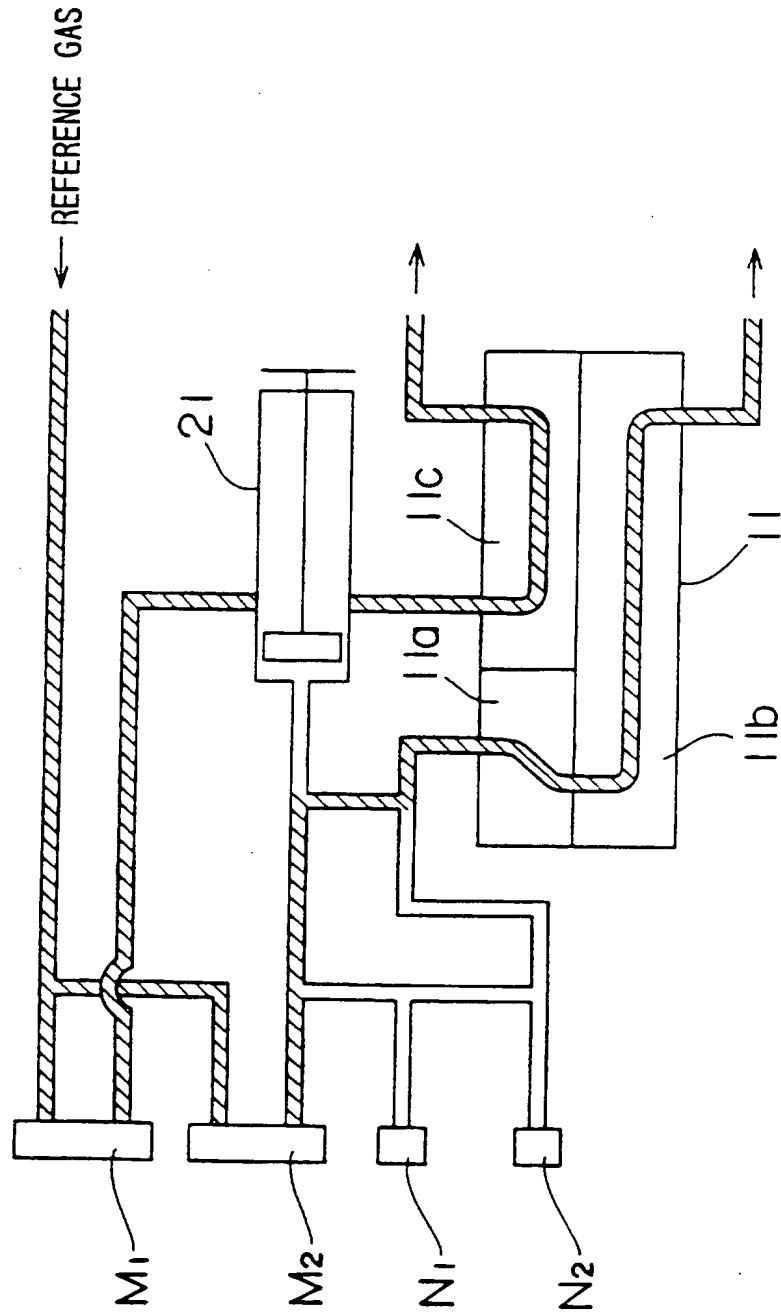
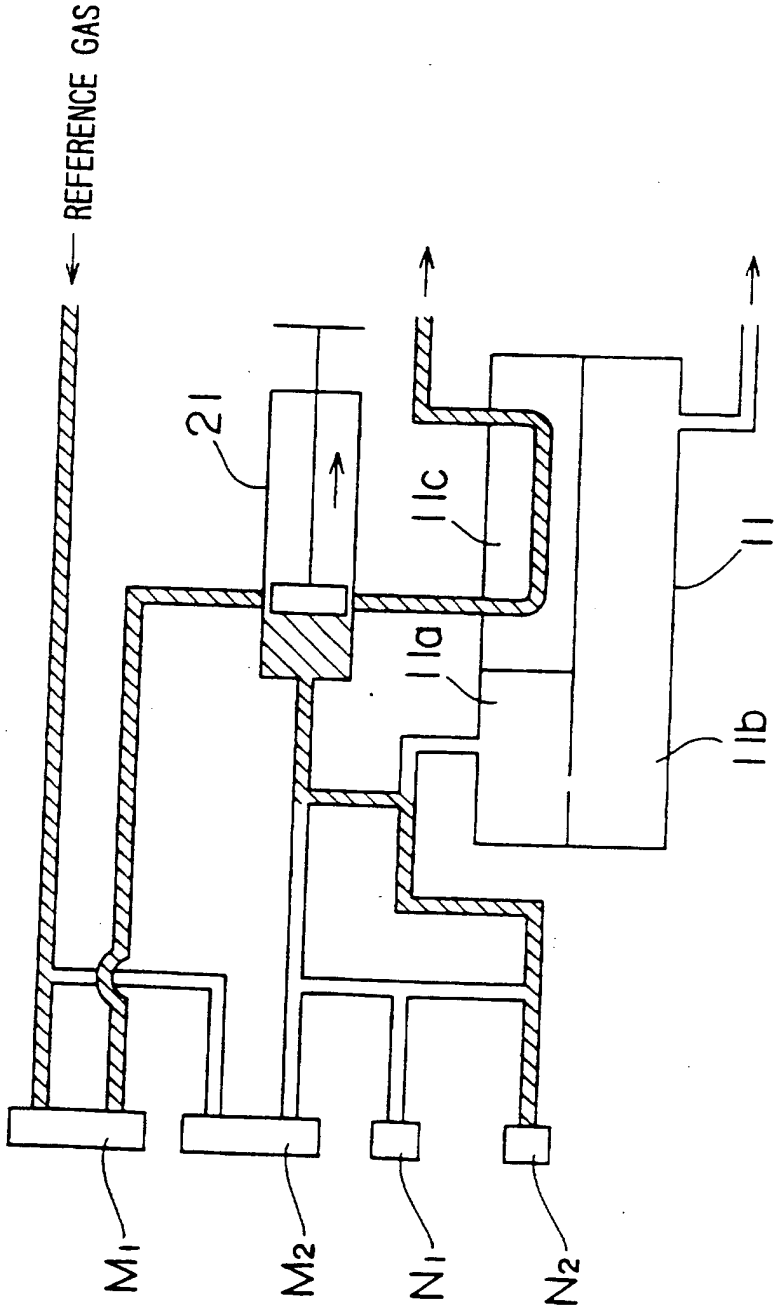


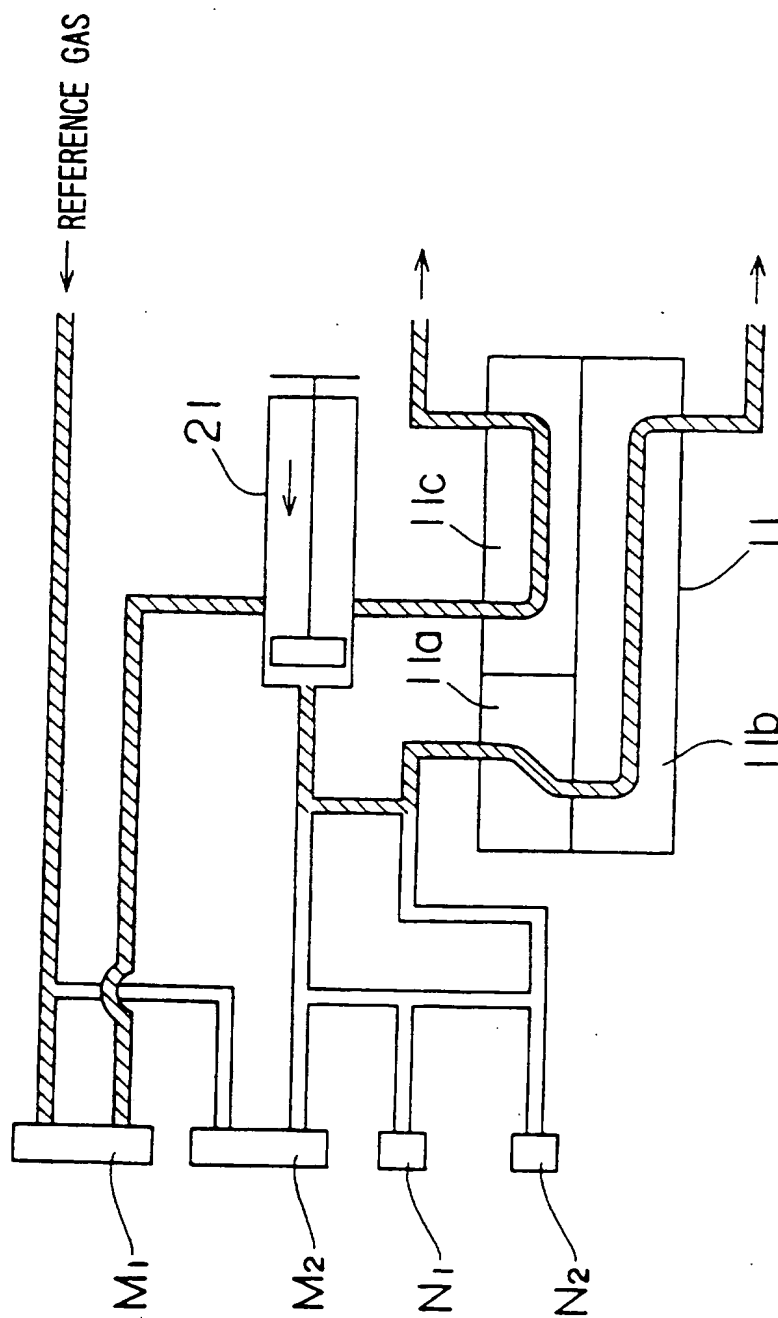
FIG. 13





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FIG. 14



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FIG. 15

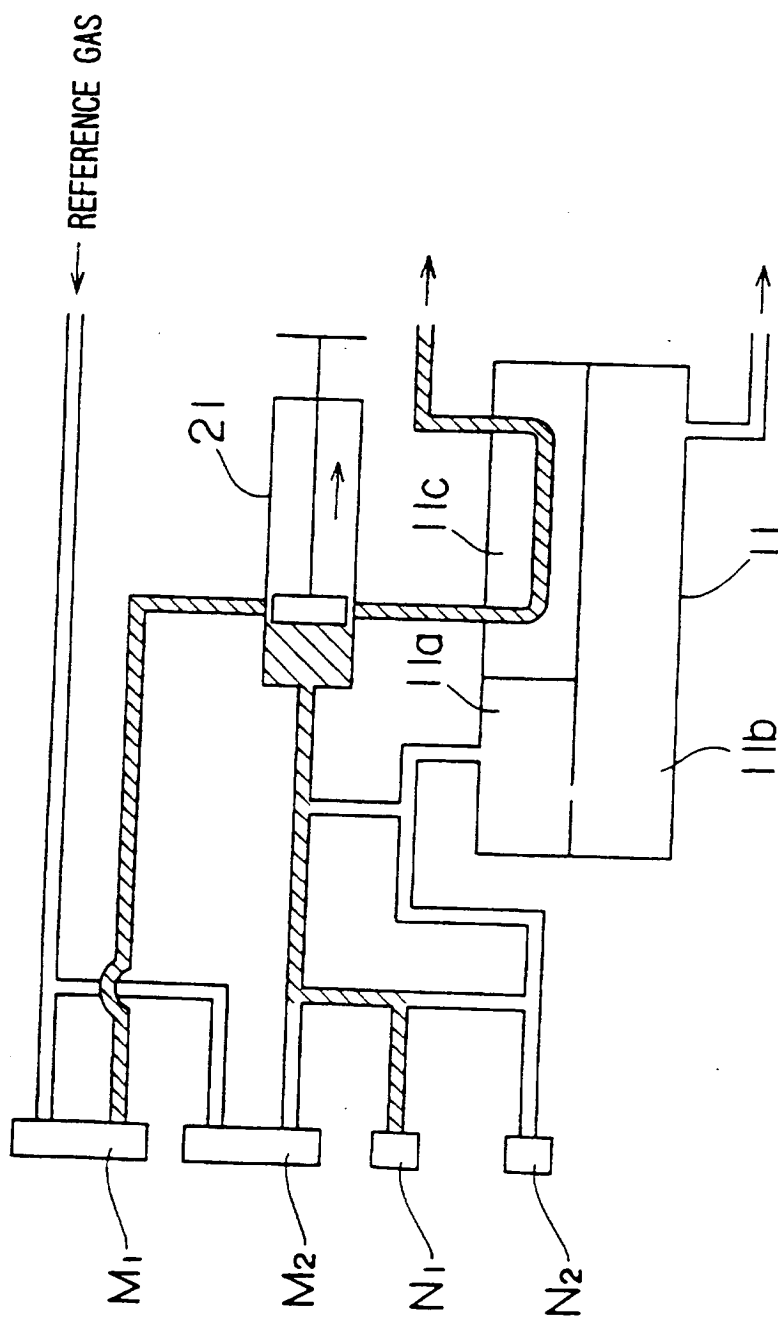
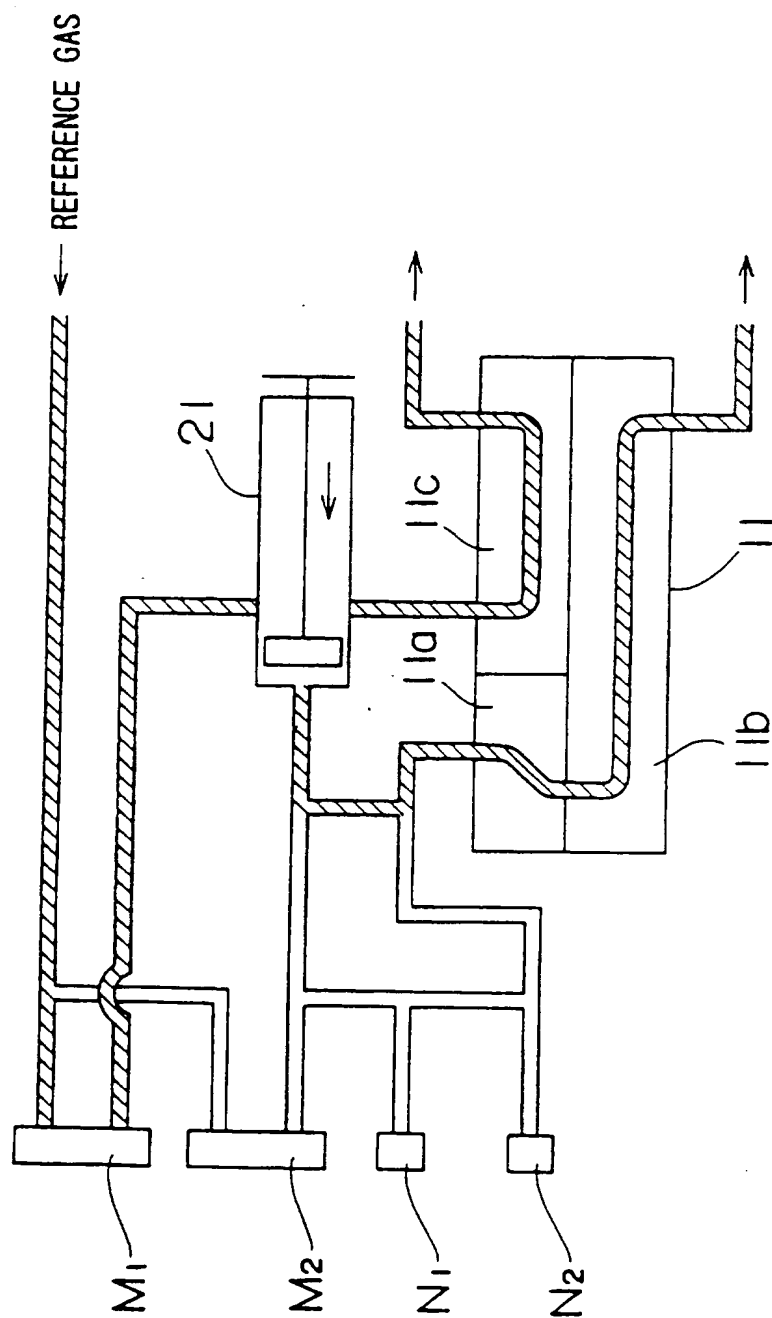


FIG. 16



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FIG. 17A

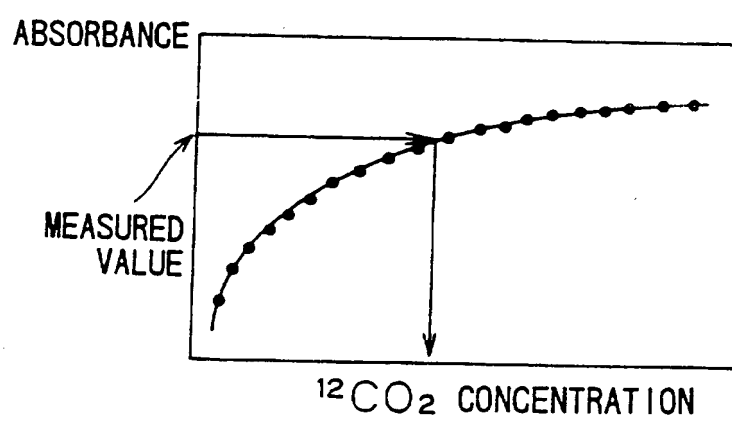
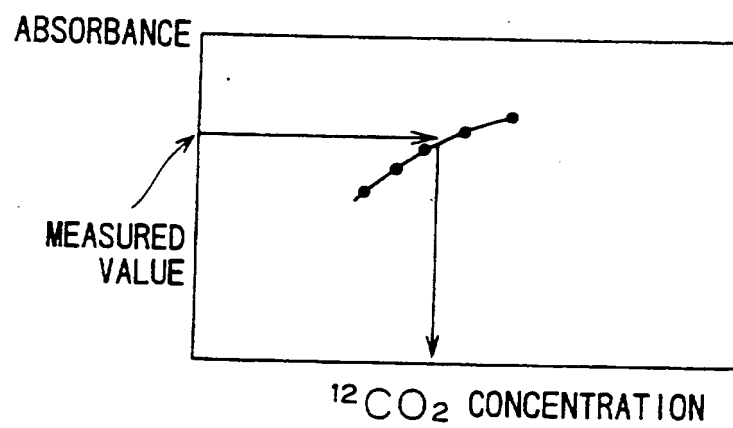


FIG. 17B



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FIG. 18A

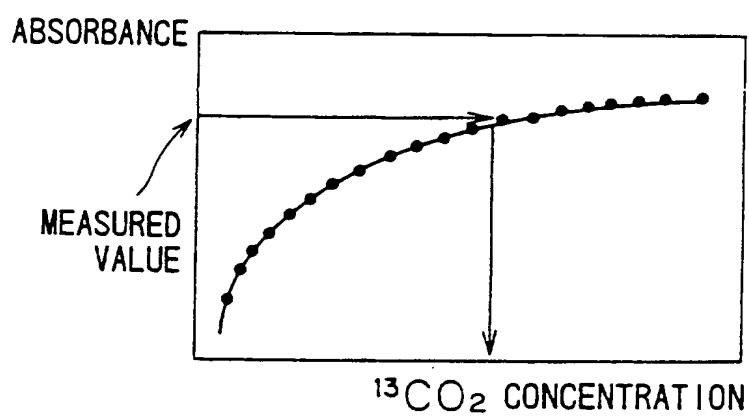
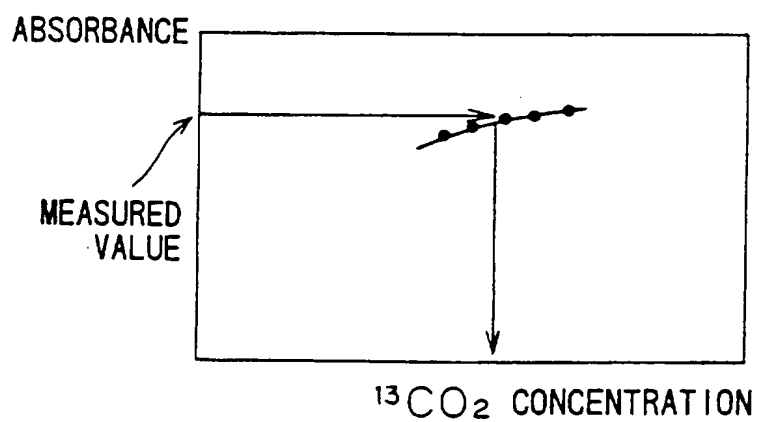
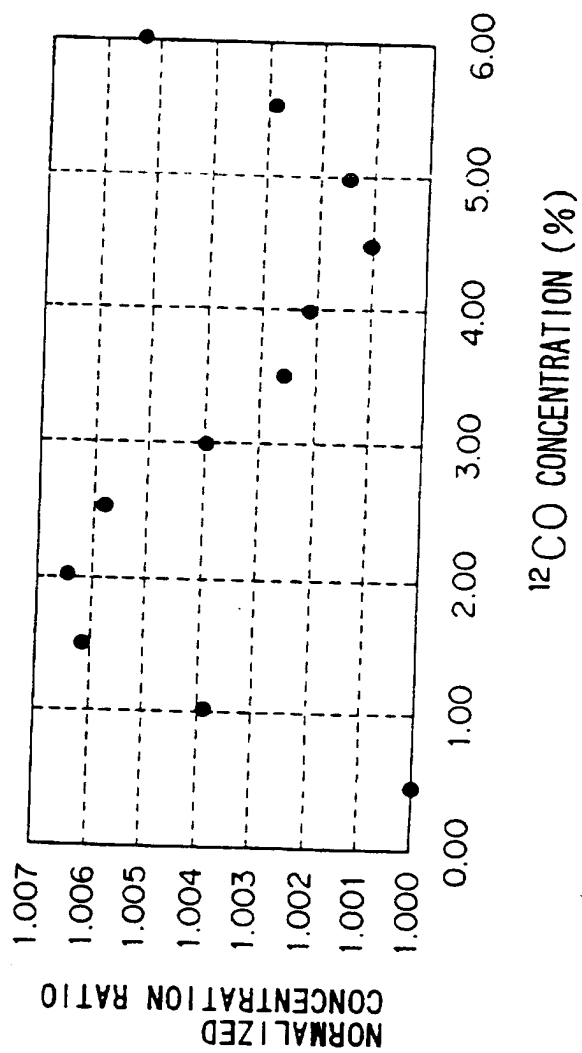


FIG. 18B



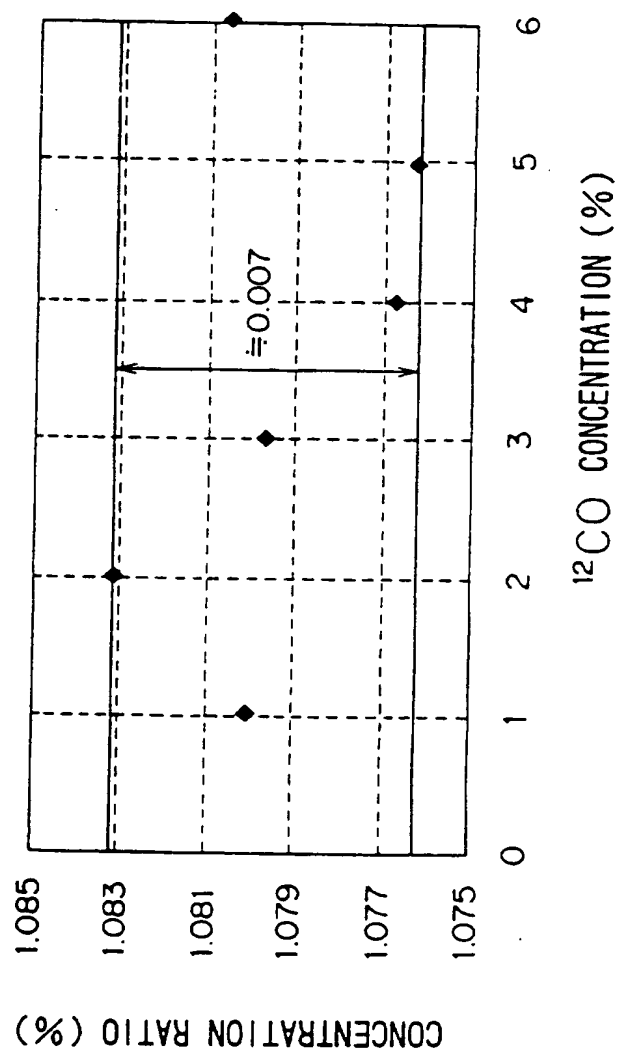
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FIG. 19



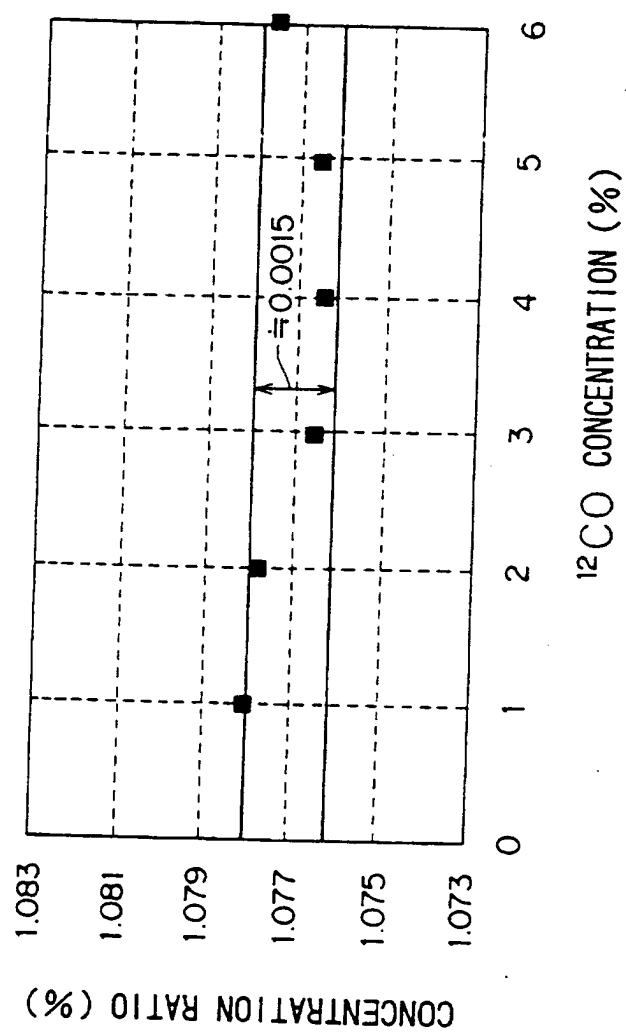
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FIG. 20



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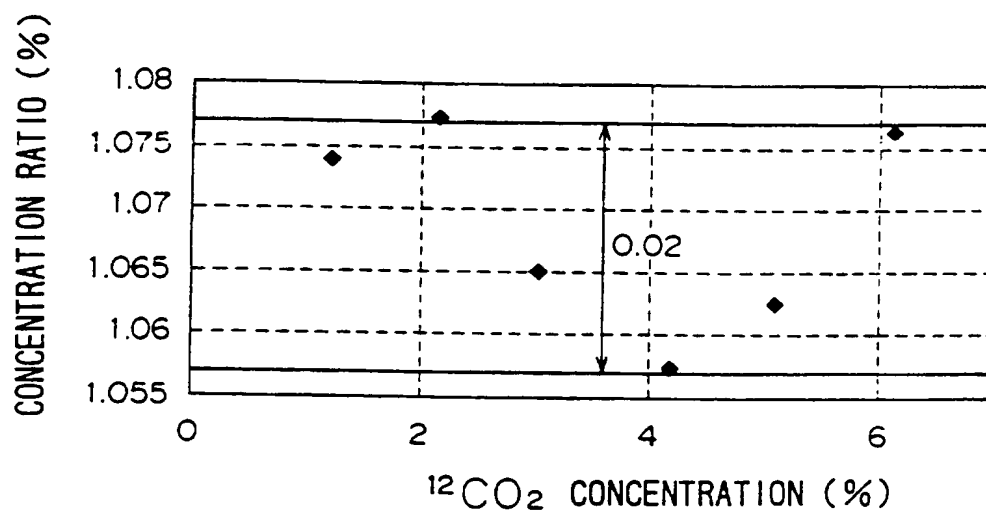
FIG. 21





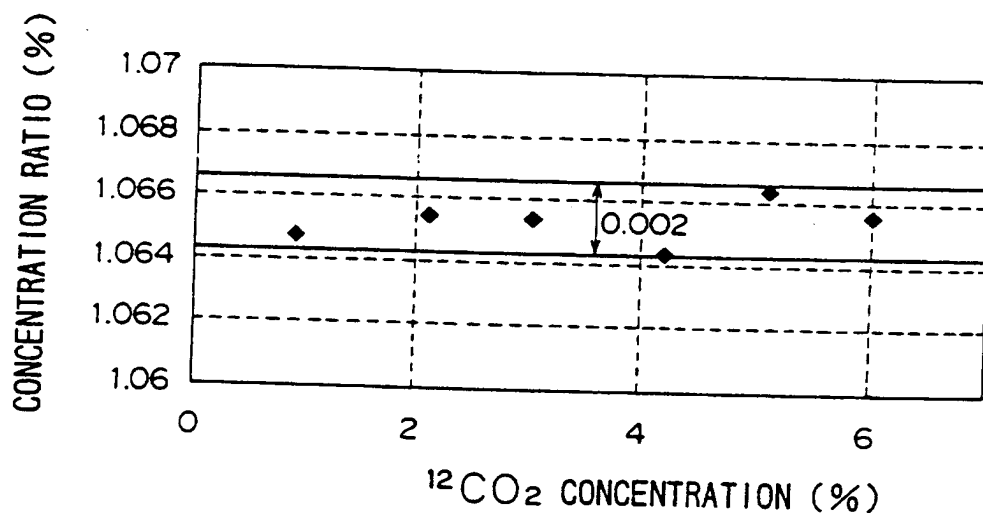
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FIG. 22



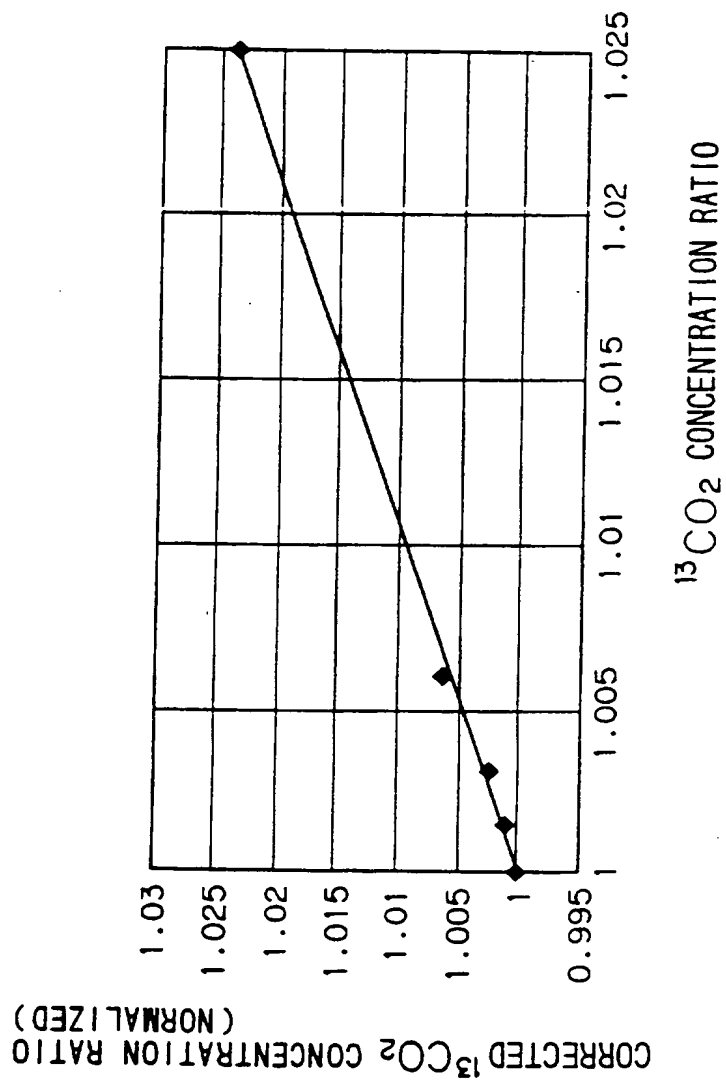
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FIG. 23



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FIG. 24



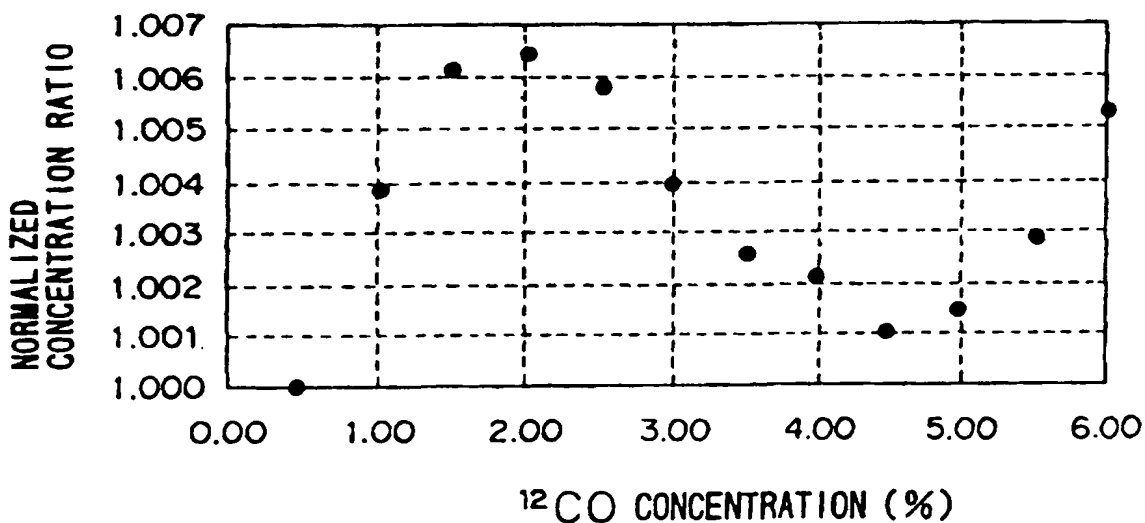




## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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(54) Title: METHOD FOR SPECTROMETRICALLY MEASURING ISOTOPIC GAS AND APPARATUS THEREOF



## (57) Abstract

A correction curve is prepared by plotting <sup>12</sup>CO<sub>2</sub> concentrations and <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratios which are determined on the basis of a calibration curve and <sup>13</sup>CO<sub>2</sub> and <sup>12</sup>CO<sub>2</sub> absorbances of gaseous samples having the same <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio but known different <sup>12</sup>CO<sub>2</sub> concentrations. A gaseous test sample containing <sup>13</sup>CO<sub>2</sub> and <sup>12</sup>CO<sub>2</sub> as component gases is introduced into a cell, and spectrometrically measured. A <sup>12</sup>CO<sub>2</sub> concentration of the gaseous test sample is determined by way of the spectrometric measurement. A concentration ratio correction value is obtained on the basis of the correction curve and the <sup>12</sup>CO<sub>2</sub> concentration of the gaseous test sample thus determined. A measured <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio is divided by the concentration ratio correction value thus obtained for correction of the <sup>13</sup>CO<sub>2</sub>/<sup>12</sup>CO<sub>2</sub> concentration ratio. Thus, the measurement accuracy of the concentration ratios of the component gases can be improved.

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# INTERNATIONAL SEARCH REPORT

Inter. Int. Application No.  
PCT/JP 96/02876

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 6 G01N21/35 A61B5/08 A61B10/00 A61B5/097

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 6 G01N A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0 584 897 A (MANNESMANN AG) 2 March 1994 see the whole document ---	1,3-7,9, 11-13,17
A	DATABASE WPI Section Ch, Week 8642 Derwent Publications Ltd., London, GB; Class B04, AN 86-277033 XP002019015 & JP 61 042 220 B (NIPPON BUNKO KOGYO KK) , 19 September 1986 cited in the application see abstract --- -/-	8-11,17, 20

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

### \* Special categories of cited documents:

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Date of the actual completion of the international search

6 March 1997

Date of mailing of the international search report

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# INTERNATIONAL SEARCH REPORT

International Application No

PCT/JP 96/02876

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	PATENT ABSTRACTS OF JAPAN vol. 010, no. 157 (P-464), 6 June 1986 & JP 61 011634 A (NIHON BUNKOU KOGYO KK), 20 January 1986, see abstract ---	12-14
X	EP 0 634 644 A (MIC MEDICAL INSTRUMENT CORPORATION) 18 January 1995 see page 1, line 1 - line 15 see page 4, line 23 - line 37; figure 1 ---	15
X	EP 0 127 259 A (BECTON, DICKINSON AND COMPANY) 5 December 1984 see page 3, line 10 - line 13 ---	27,28
Y	see page 5, line 10 - line 27	26
A	see page 6, line 15 - line 19 see page 8, line 1 - line 14; figures 1,3 ---	15,25
Y	US 5 131 387 A (G.H. FRENCH ET AL.) 21 July 1992 see abstract ---	26
X	US 3 544 273 A (MC CONNAUGHEY PAUL W) 1 December 1970 ---	25
A	see column 1, line 52 - line 59; figures ---	23,24
X	US 3 734 692 A (LUCKER J ET AL) 22 May 1973 see column 3, line 58 - line 64; figures ---	25
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X	DE 19 15 540 A (E. JAEGER) 1 October 1970 see page 3, line 17 - line 25; figure ---	27
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P,A	US 5 543 621 A (SAUKE TODD B ET AL) 6 August 1996 see column 8, line 64 - column 10, line 50; claims 1,2,4,7 -----	1,3-11, 17,19,22



# INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP 96/02876

## Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:  
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:  
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. Claims 1-14, 17-22
2. Claims 15, 16
3. Claims 23, 24, 27, 28
4. Claims 25
5. Claim 26

1. ☒ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
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4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☒ No protest accompanied the payment of additional search fees.

# INTERNATIONAL SEARCH REPORT

information on patent family members

International Application No

PCT/JP 96/02876

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